

Introduction à la Microscopie à Force Electrostatique

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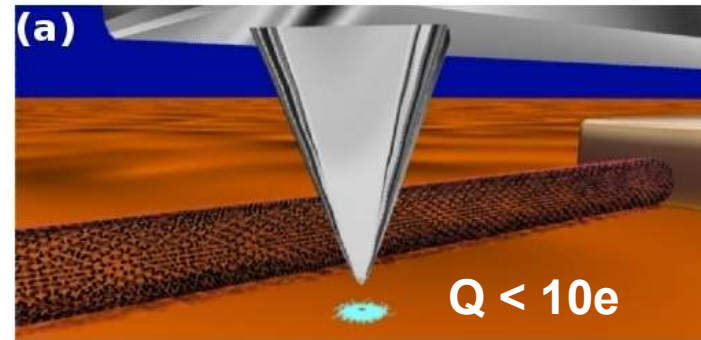
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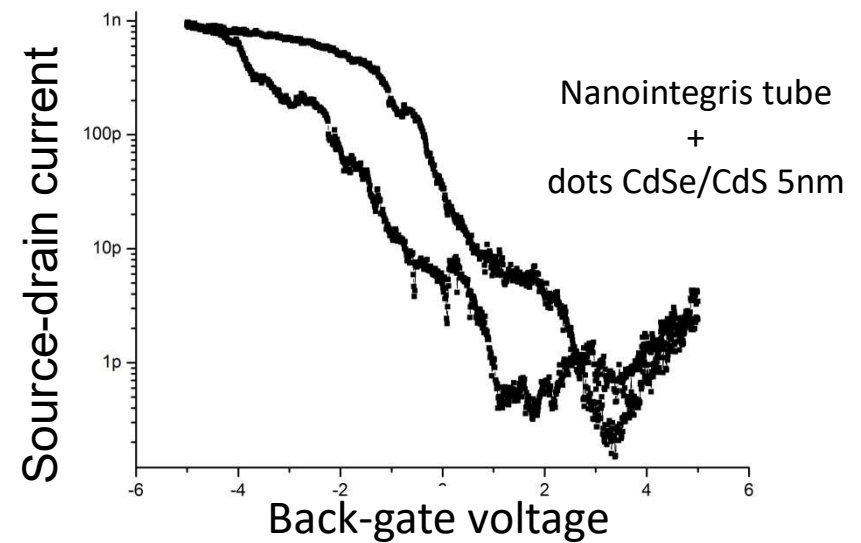
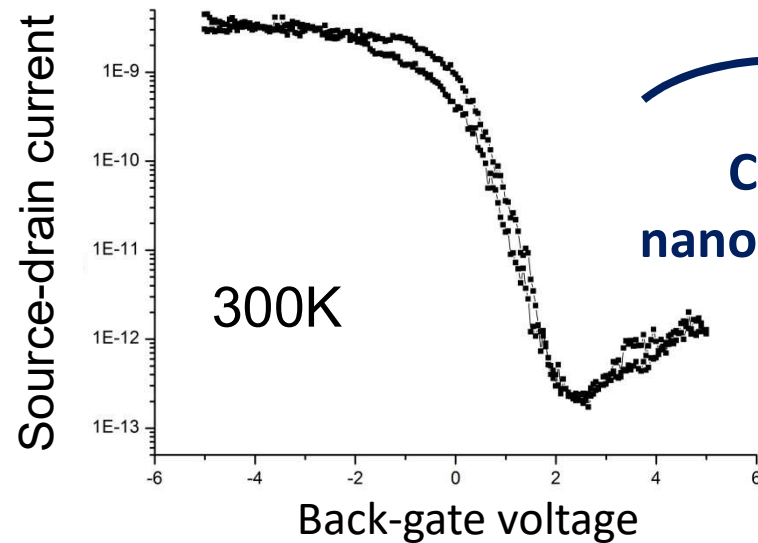
A few motivations

EX 1 : Imaging the operation of CNT-FETs as charge sensors

[D. Brunel et al., ACS Nano 2010]

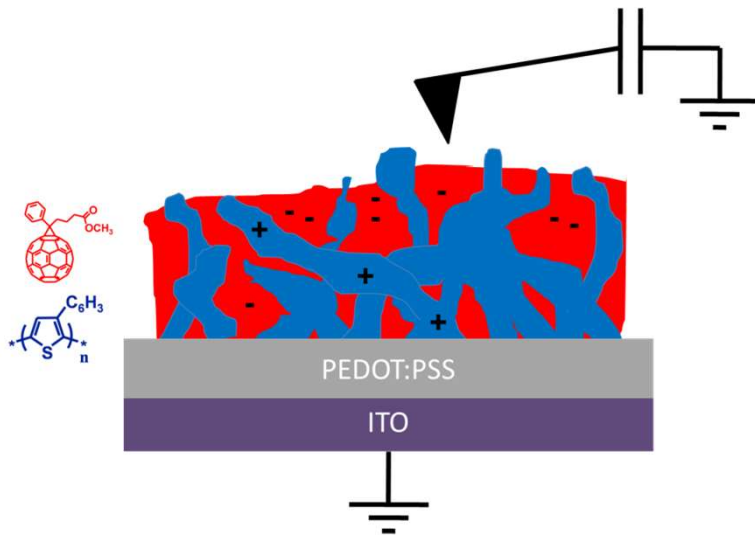


EX 2 : coupled CNTFETs and nanocrystals

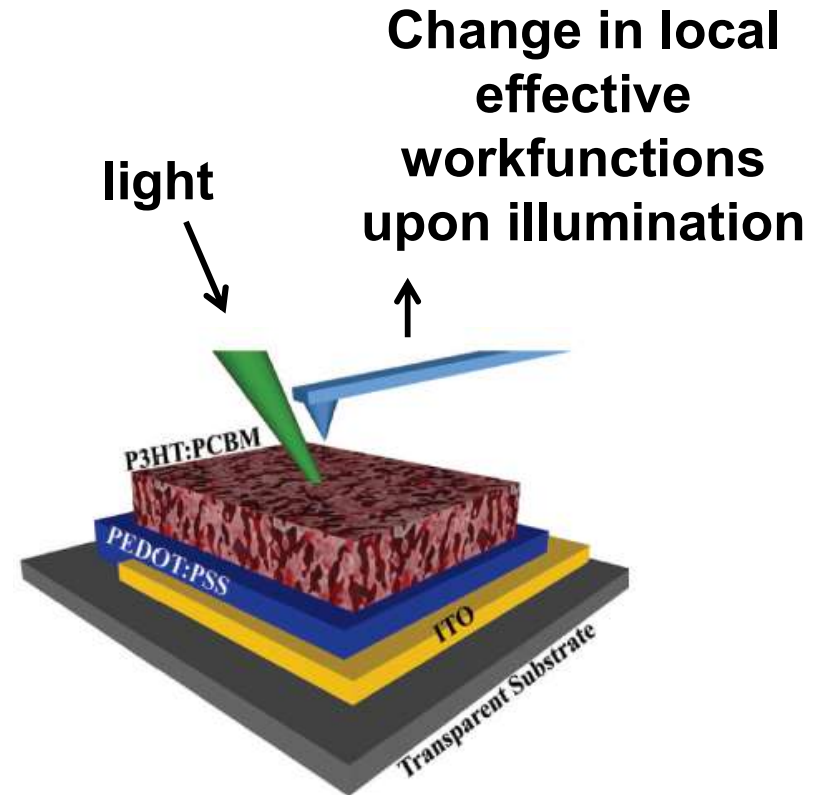


A few motivations

EX 3 : photovoltaic materials



P3HT:PCBM blend
molecular D/A junction



cf Ł. Borowik / B. Grévin

EFM

Electrostatic Force Microscopy

Measurement of electrostatic force gradient

Units : Hz or N/m

KPFM

Kelvin Probe Force Microscopy

Compensation of electrostatic force (gradient)

Units : V

Charge detection



Probing local surface potential



SOMMAIRE

Quelques rappels : force capacitive & CPD

Microscopie à force électrostatique (EFM)

Détection de charge(s) ?

Microscopie à sonde de Kelvin (KFM)

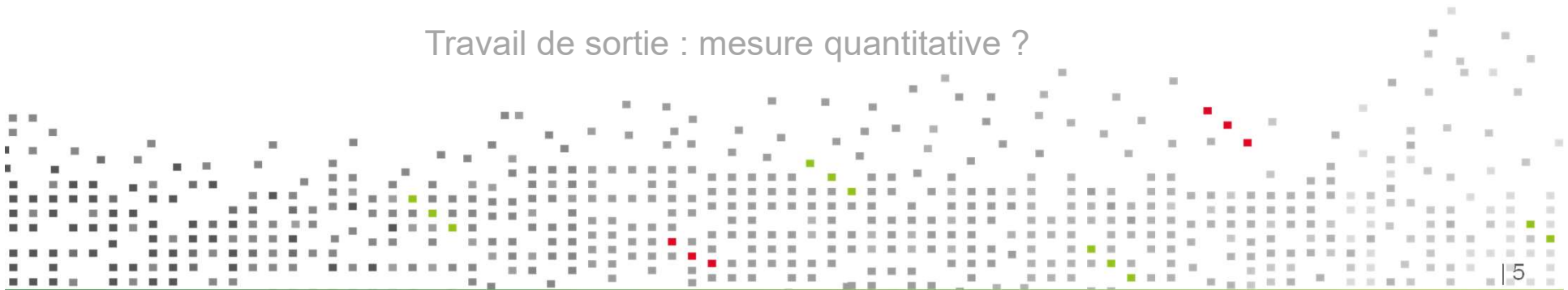
Modulation d'Amplitude (AM) vs Modulation de Fréquence (FM)

Effet des capacités latérales

Acquisition en boucle ouverte (OL-KFM)


KFM & DFRT (Dual Frequency Resonant Tracking)

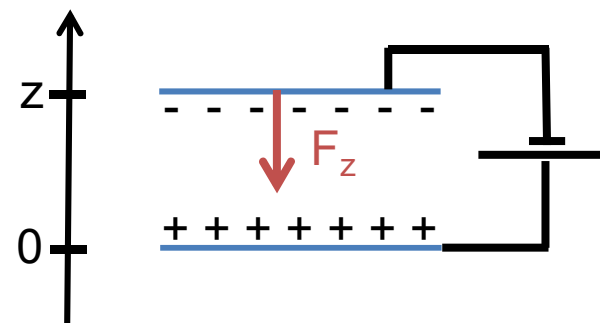
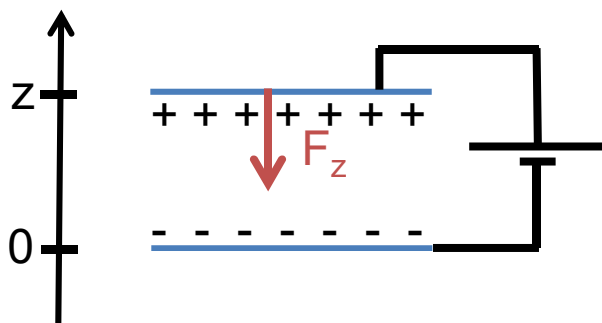
Travail de sortie : mesure quantitative ?



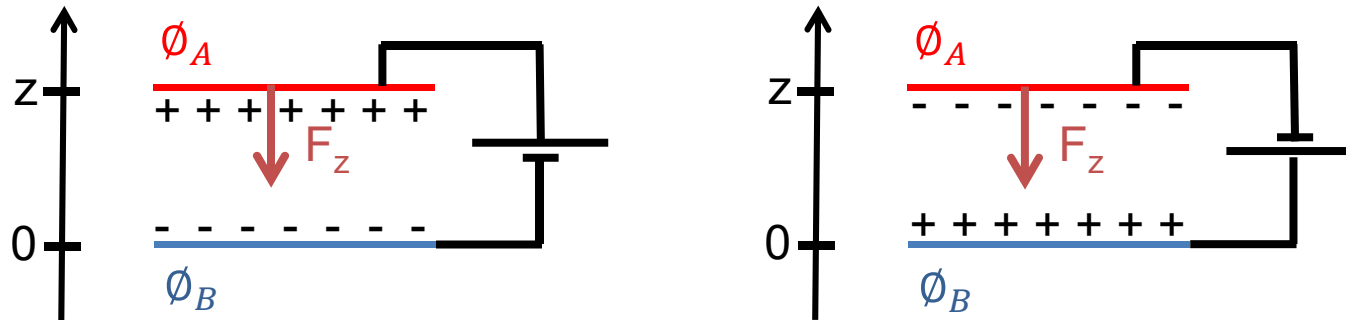
Energy stored in a capacitor $\frac{1}{2} C V^2$

Attractive force between capacitor plates

 $F_z = + \underbrace{\frac{1}{2} \frac{\partial C}{\partial z}}_{<0} V^2 < 0$



Capacitor with 2 ≠ plates

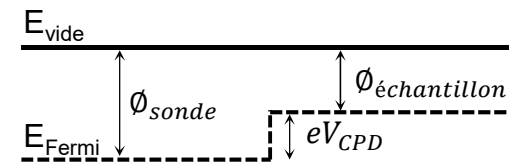
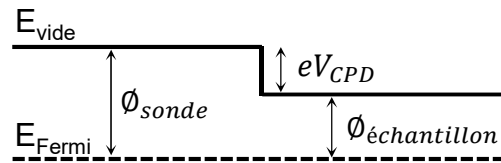
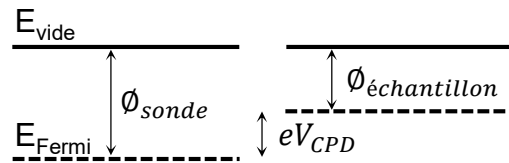
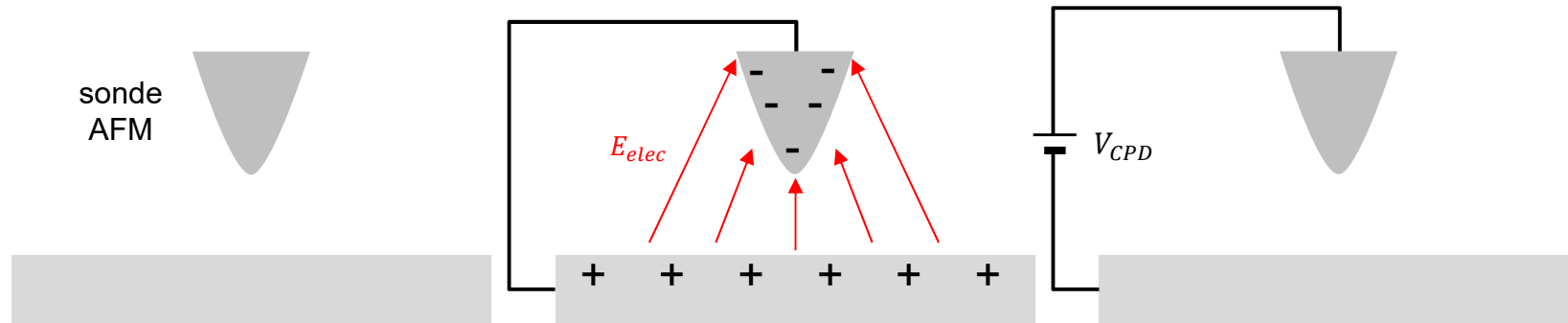


Contact potential difference $V_{CPD} = \frac{\Phi_A - \Phi_B}{|e|}$

$$F_z = + \frac{1}{2} \frac{\partial C}{\partial z} (V \pm V_{CPD})^2 < 0$$

V applied to *plate A* → -
 V applied to *plate B* → +

FORCE ÉLECTROSTATIQUE (CAPACITIVE) EN AFM



$$V_{CPD} = \frac{\phi_{sonde} - \phi_{echantillon}}{|e|}$$

Différence de potentiel de contact



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Détection de charge(s) ?

Microscopie à sonde de Kelvin (KFM)

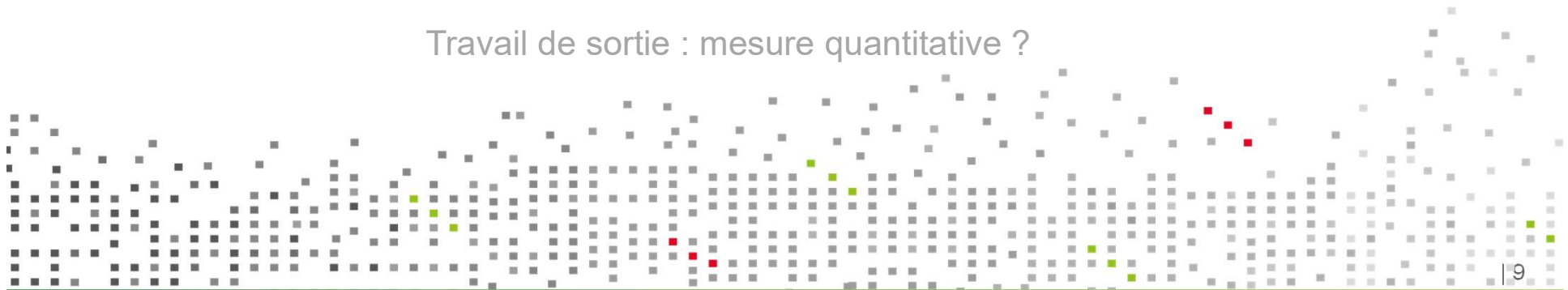
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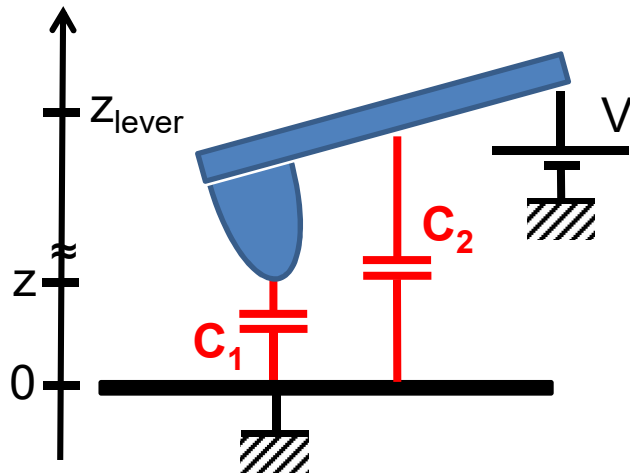
KFM & DFRT (Dual Frequency Resonant Tracking)

Travail de sortie : mesure quantitative ?



Charge $\{\equiv \text{capacitance}\}$

$$V_{CPD} = 0$$



$$Q = C.V$$

Tip apex

$$C_1 \approx 4\pi\epsilon_0 R_{apex}$$

$$R_{apex} = 20\text{nm}$$

$$z \gg R_{apex}$$

$$Q_1 \approx 20 e$$

Cantilever

$$C_2 \approx \epsilon_0 S_{lever} / z_{lever}$$

$$S_{lever} = 30\mu\text{m} \times 100\mu\text{m}$$

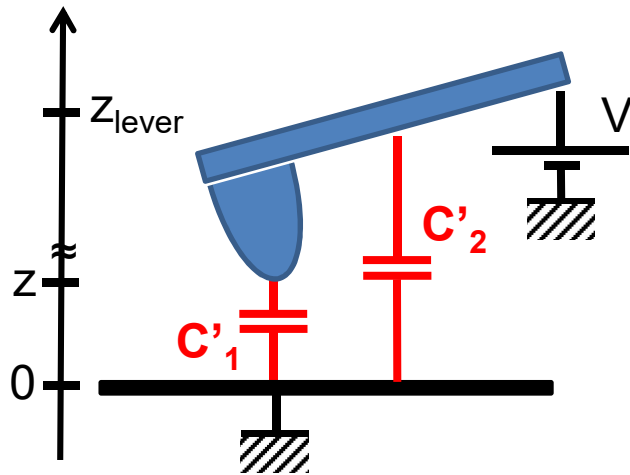
$$z_{lever} = 15\mu\text{m}$$

$$Q_2 \approx 10^4 e$$

$$[V=1V]$$

Electrostatic Force {≡ capacitance gradient}

$$V_{CPD} = 0$$



Attractive force between capacitor plates

$$F_z = + \frac{1}{2} \frac{\partial C}{\partial z} V^2 < 0$$

Tip apex

Cantilever

$$|dC_1/dz| \approx 4\pi\epsilon_0 R_{\text{apex}}^2 / z^2$$

$$|dC_2/dz| \approx \epsilon_0 S_{\text{lever}} / z_{\text{lever}}^2$$

$$R_{\text{apex}} = 20\text{nm}$$

$$z = 100\text{nm}$$

$$S_{\text{lever}} = 30\mu\text{m} \times 100\mu\text{m}$$

$$z_{\text{lever}} = 15\mu\text{m}$$

[V=1V]

$F_1 \approx 5 \text{ pN}$

$F_2 \approx 100 \text{ pN}$

Force gradient detection

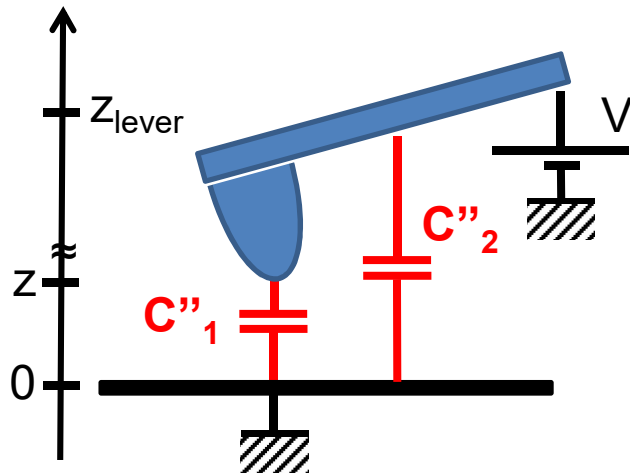
$$F_z = F_z \Big|_{z_0} + (z - z_0) \underbrace{\frac{\partial F_z}{\partial z} \Big|_{z_0}}$$

Frequency shift : $\Delta f \cong -\frac{f_\infty}{2k} \frac{\partial F_z}{\partial z} \Big|_{z_0}$

- Here: long-range forces [ambient air / UHV]
- Short-range electrostatic forces disregarded here

Force gradient $\{\equiv \text{capacitance } 2^{\text{nd}} \text{ derivative}\}$

$$V_{CPD} = 0$$



$$\text{force gradient } \frac{\partial F_z}{\partial z} = + \frac{1}{2} \frac{\partial^2 C}{\partial z^2} V^2$$

Tip apex

Cantilever

$$d^2C_1/dz^2 \approx 8\pi\epsilon_0 R_{\text{apex}}^2 / z^3$$

$$d^2C_2/dz^2 \approx 2\epsilon_0 S_{\text{lever}} / z_{\text{lever}}^3$$

$$R_{\text{apex}} = 20\text{nm}$$

$$z = 100\text{nm}$$

$$S_{\text{lever}} = 30\mu\text{m} \times 100\mu\text{m}$$

$$z_{\text{lever}} = 15\mu\text{m}$$

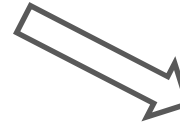
$$[V=1\text{V}] \quad dF_1/dz \approx 10^{-4} \text{ N/m} \quad dF_2/dz \approx 2 \cdot 10^{-5} \text{ N/m}$$

dF_1/dz (apex) exceeds dF_2/dz (cantilever)

MESURE DU GRADIENT DE FORCE ÉLECTROSTATIQUE ?

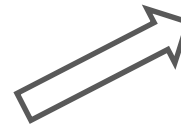
- Par le décalage de phase (mécanique):

$$\Delta\varphi \cong -\frac{Q}{k} \frac{\partial F_z}{\partial z} \Big|_{z_0} = -\frac{Q}{2k} \frac{\partial^2 C}{\partial z^2} \Big|_d (V \pm V_{CPD})^2$$



- Par le décalage de fréquence:

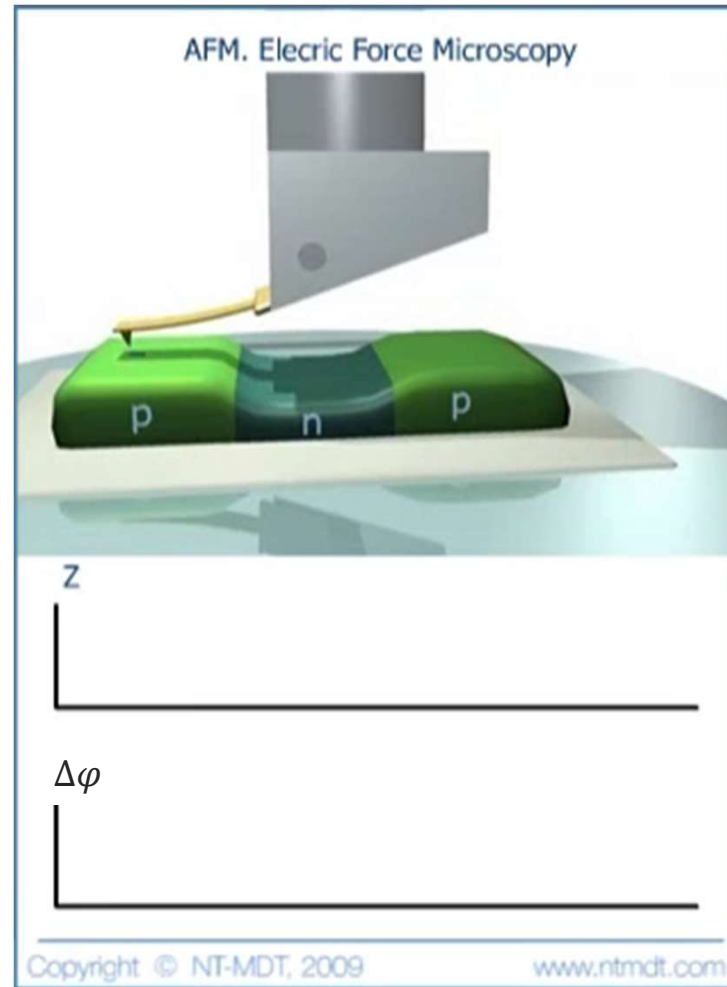
$$\Delta f \cong -\frac{f_\infty}{2k} \frac{\partial F_z}{\partial z} \Big|_{z_0} = -\frac{f_\infty}{2k} \frac{\partial^2 C}{\partial z^2} \Big|_d (V \pm V_{CPD})^2$$



$$\frac{\Delta\varphi}{\Delta f} = \frac{2Q}{f_\infty}$$

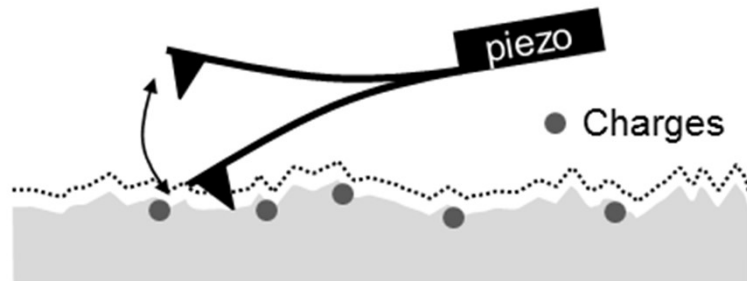
EFM \equiv mesure du décalage de fréquence ou de phase

ACQUISITION EFM



ACQUISITION EFM

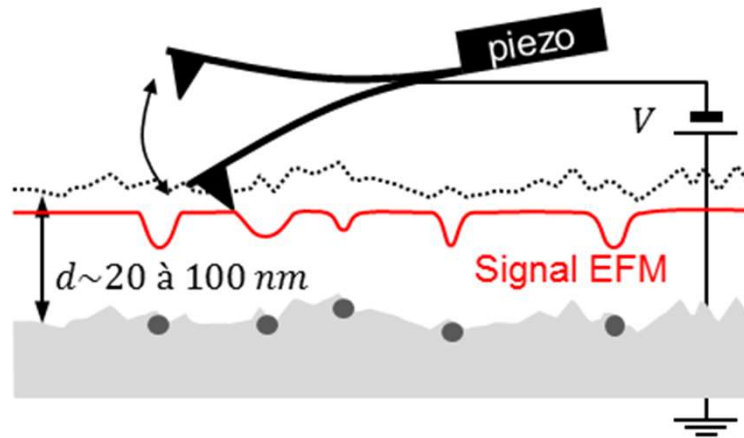
1^{er} passage : topographie



Excitation mécanique à la résonance du levier f_0

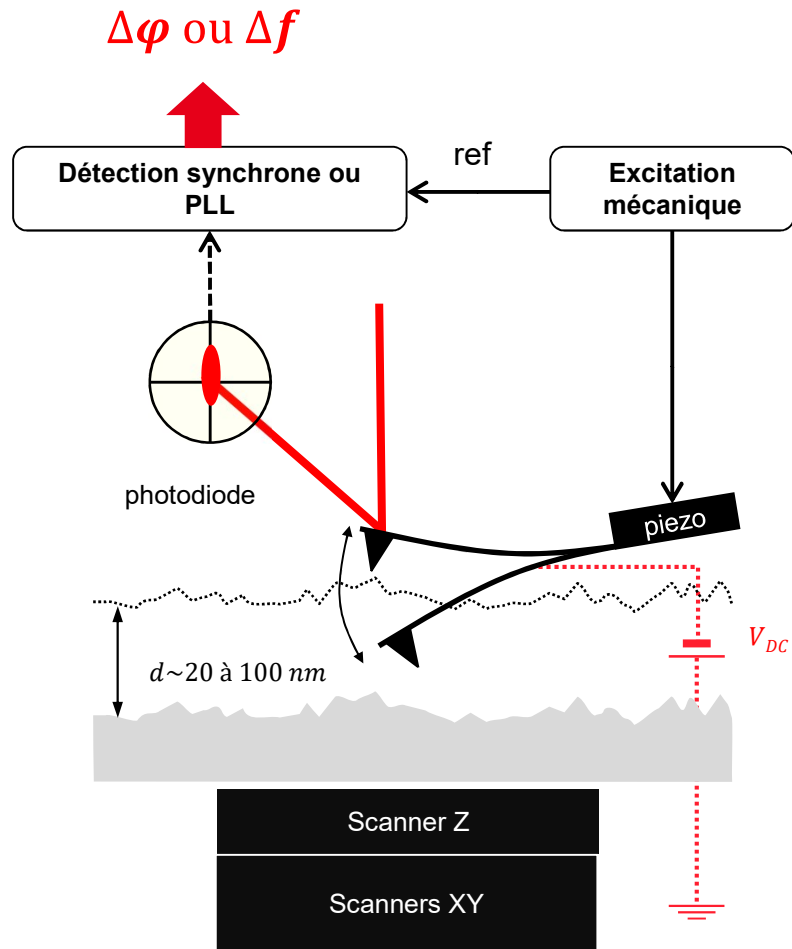
Tapping (Air) ou nc-AFM (Vide, UHV)

2^{ème} passage : EFM

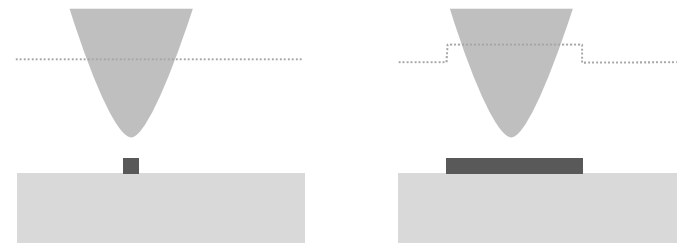


Excitation mécanique à la résonance du levier f_0 + tension continue V_{DC}

Hauteur de lift (20 à 100 nm)



- Lors du mode lift : **excitation mécanique à la résonance du levier f_0 + tension continue V_{DC}**
- Modes : imagerie ou spectroscopie
- Distance ou altitude constante ?





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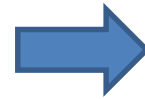
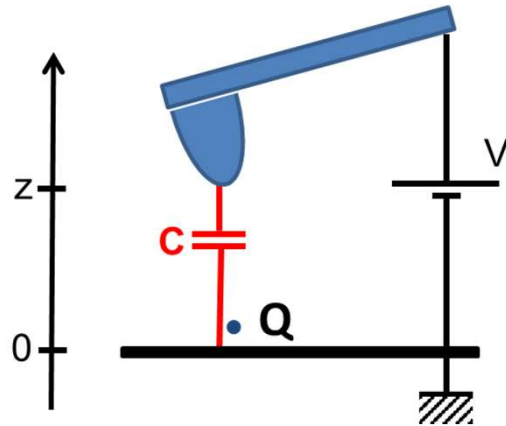
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Travail de sortie : mesure quantitative ?

Charge in a capacitor



V_Q effective surface potential

$$\frac{\partial F_z}{\partial z} = + \frac{1}{2} \frac{\partial^2 C}{\partial z^2} \left[(V - V_{CPD})^2 - 2(V - V_{CPD})V_Q + V_Q^2 \right]$$

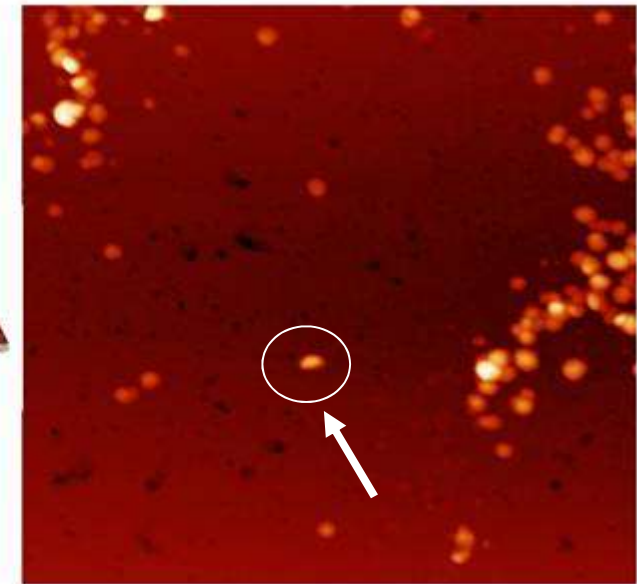
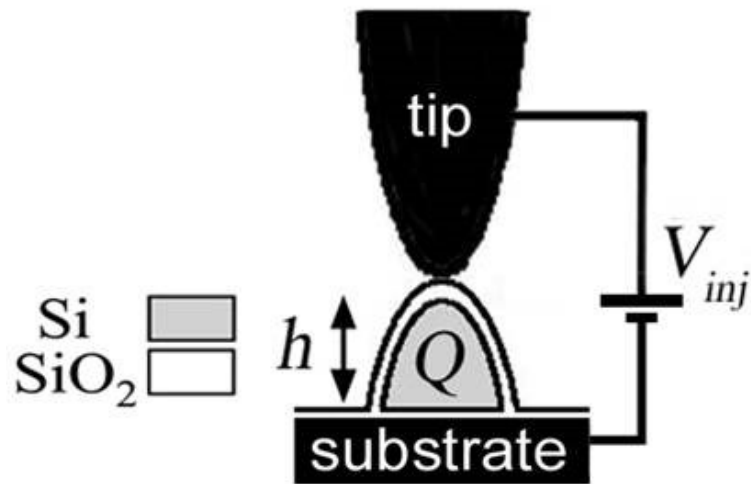
Capacitive force gradient $\propto V^2$

Charge interaction $Q \Leftrightarrow$ probe charge $\propto Q \cdot V$
determination of the sign of the surface charge Q

Image charge effect $\propto Q^2$

How to discriminate these electrostatic contributions ?

Example 1 : Charge manipulation

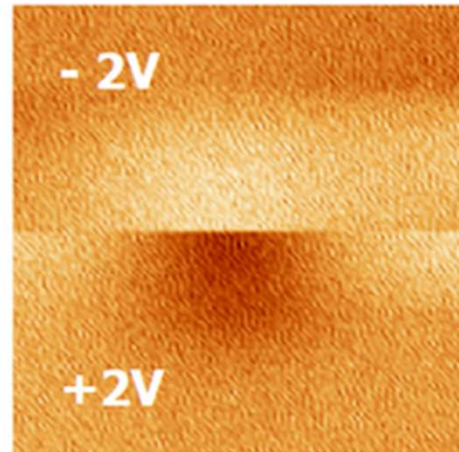
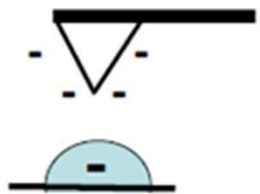


AFM Image 2500 x 2500 nm²

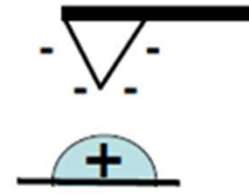
Contact force : a few nN

Charge retention time : of few 10 min (dry N₂)

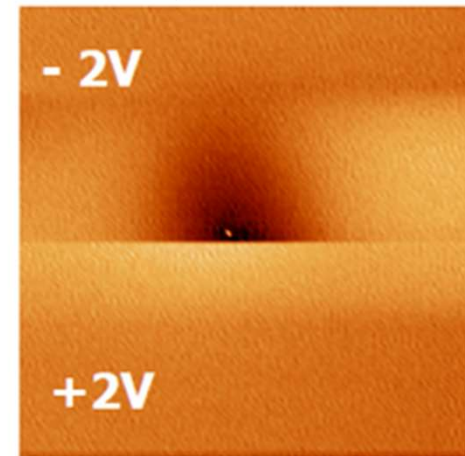
Example 1 : Imaging charged nanocrystals



**Injection @ -6V
($\sim -150 e$)**

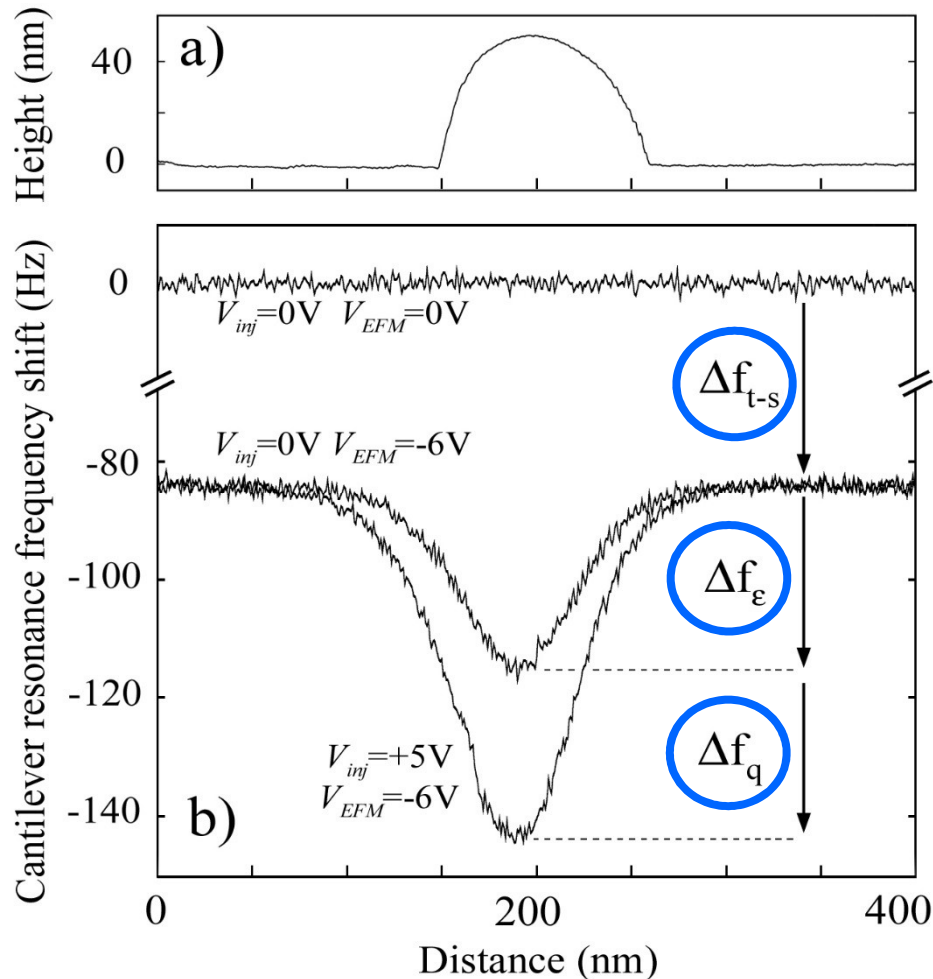


EFM (Δf_0) 300x300nm



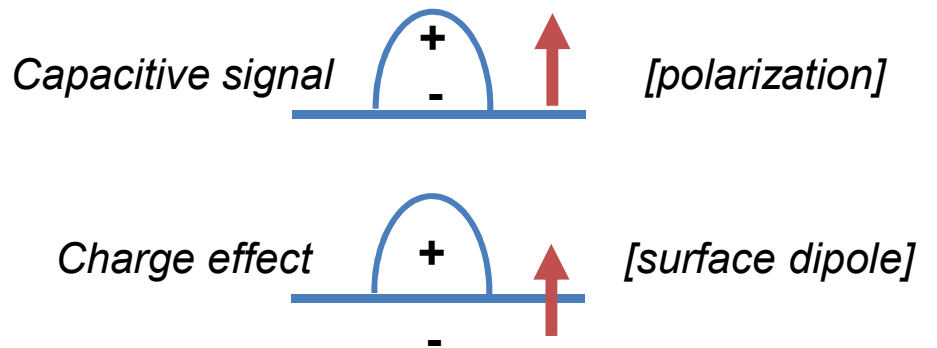
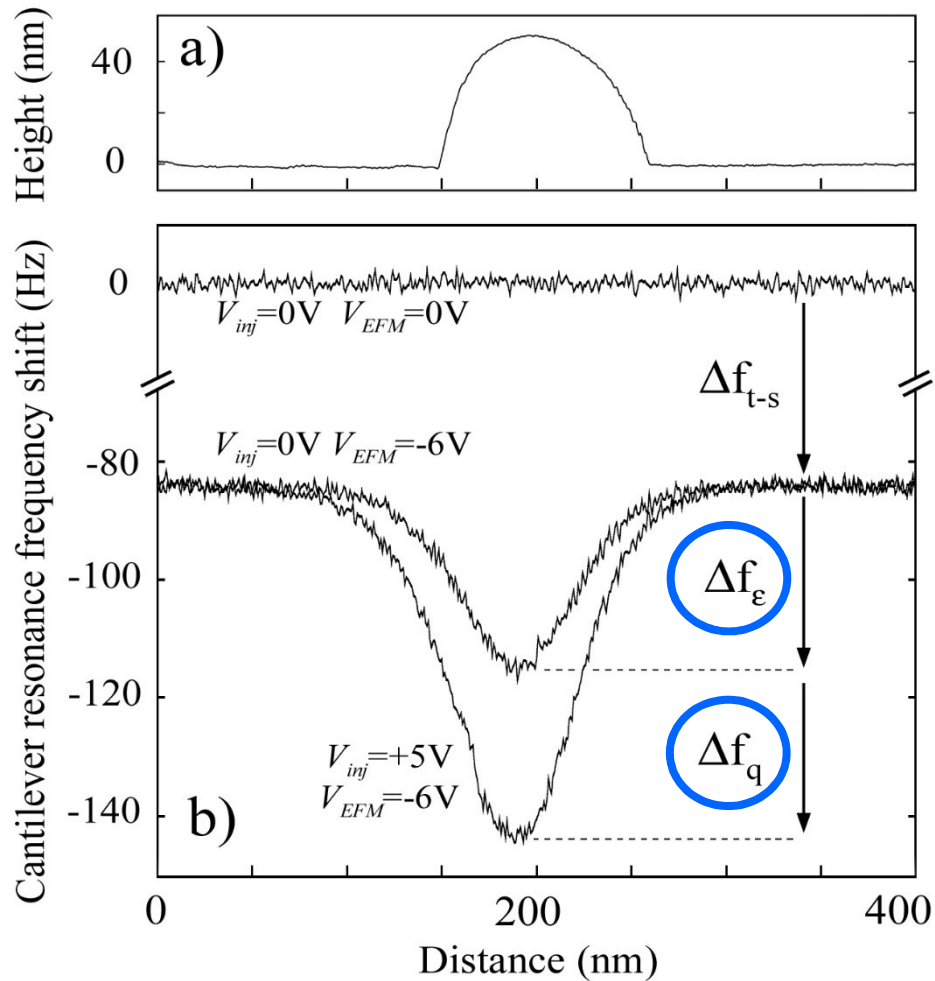
**Injection @ +6V
($\sim +150 e$)**

Example 1 : Probing a charge or a dipole ?

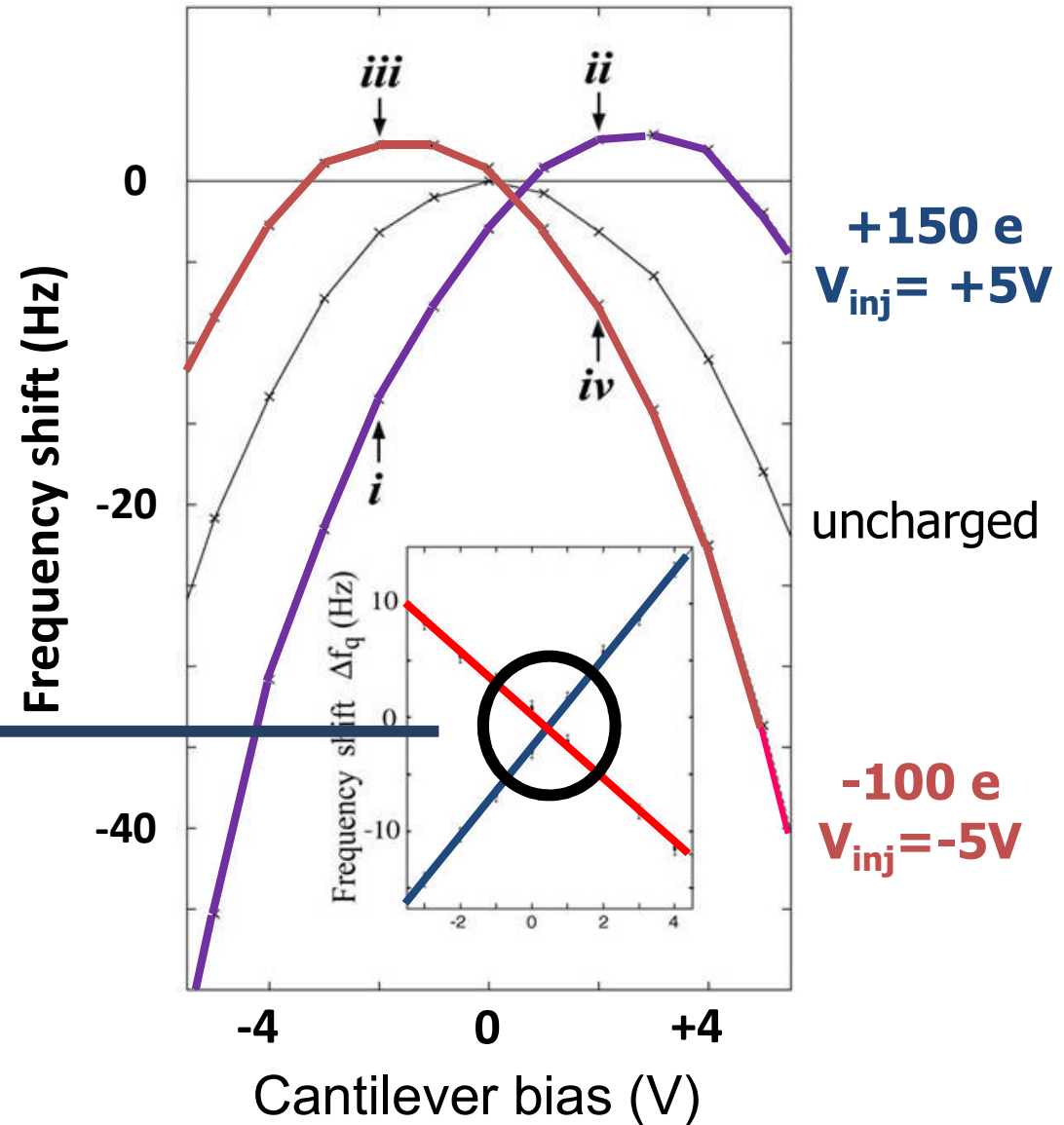
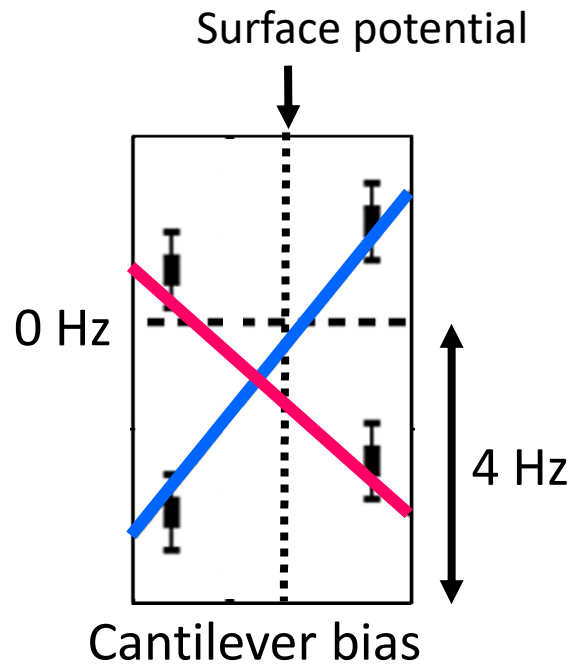
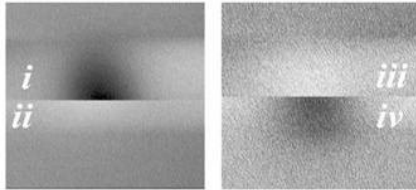


- tip-substrate capacitance
prop. to V^2
- nanoparticle capacitive effect
prop. to V^2
- charge perturbation
prop. to $Q.V$ (+ Q^2 contribution)

Example 1 : Probing a charge or a dipole ?

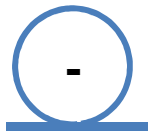


Example 1 : Spectroscopic analysis of charge signals



Example 2 : Probing a charge or a dipole ?

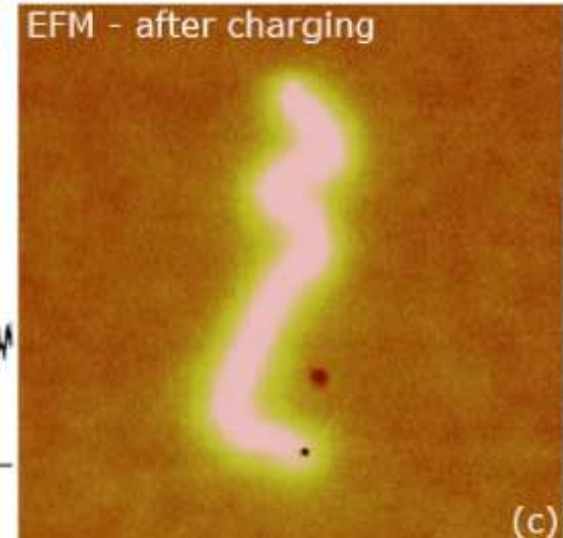
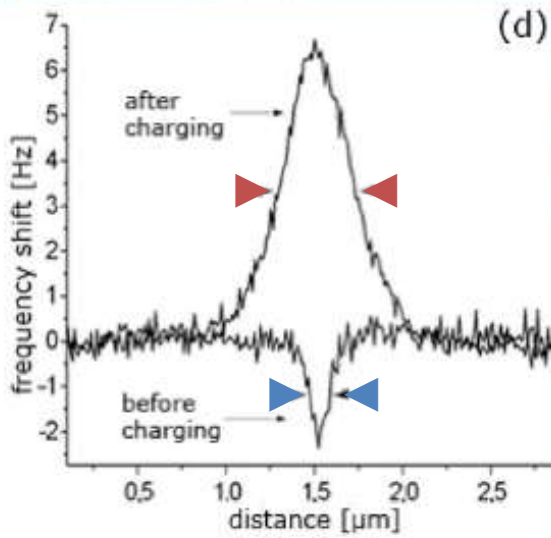
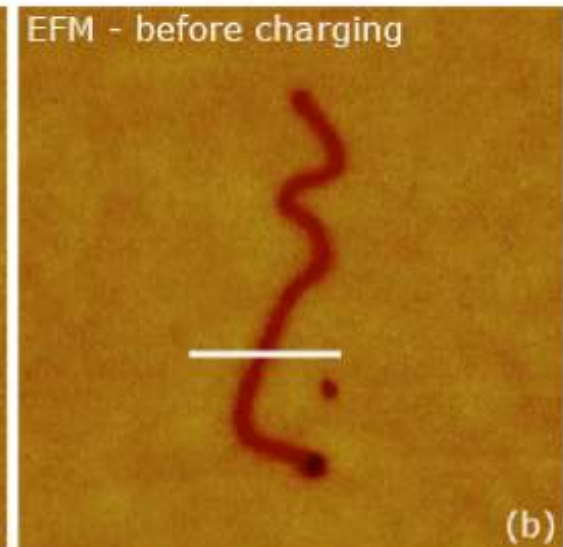
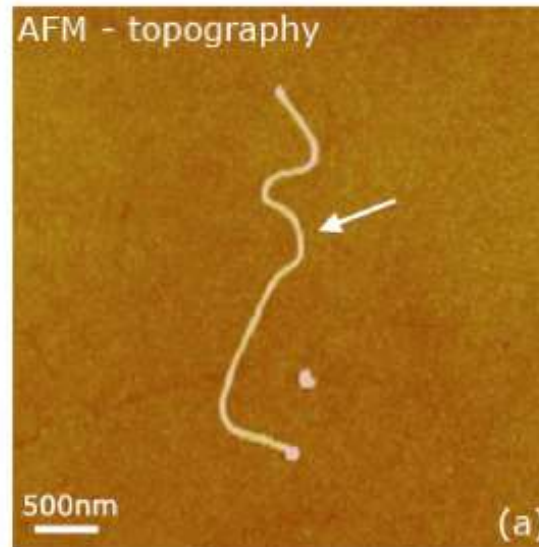
multiwalled carbon nanotube MWCNT
(~20nm diameter)
on 200nm thick SiO₂



charge signal

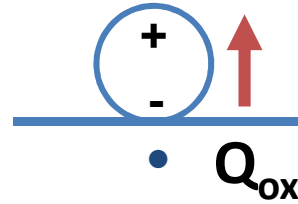


capacitive signal



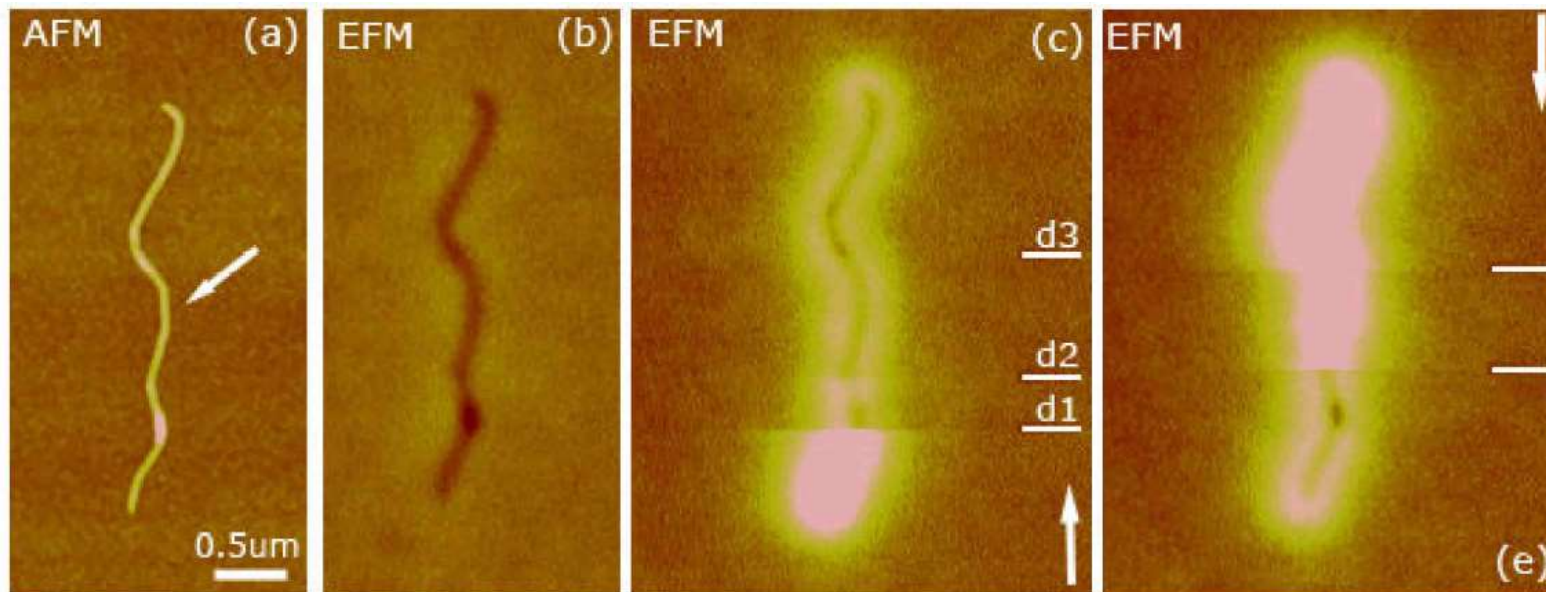
Example 2 : Probing a charge or a dipole ?

After discharge



capacitive signal

+ residual oxide charge



[MWCNT with 18 nm diameter, $V_{inj}=-7V$ (3 min) detection $V_{EFM}=-3V$]

Sensitivity

Optical beam deflection EFM
with soft cantilevers ($k=3\text{N/m}; f_0=60\text{kHz}$)

	in air	in vacuum, 300K
F'_{\min}	limited by thermal noise	
	<p>$\sim 10^{-5} \text{ N/m}$</p> <p>B=100Hz, Q=200 A=25nm</p>	<p>a few 10^{-6} N/m</p> <p>B=50Hz, Q=20000 A=15nm</p>
$\langle z \rangle$	50-100nm	10-20nm

$$F'_{\min} = \sqrt{\frac{4 k \cdot k_B T \cdot B}{\pi f_0 \cdot A^2 \cdot Q}}$$

Sensitivity

Optical beam deflection EFM
with soft cantilevers ($k=3\text{N/m}; f_0=60\text{kHz}$)

Qplus, LER

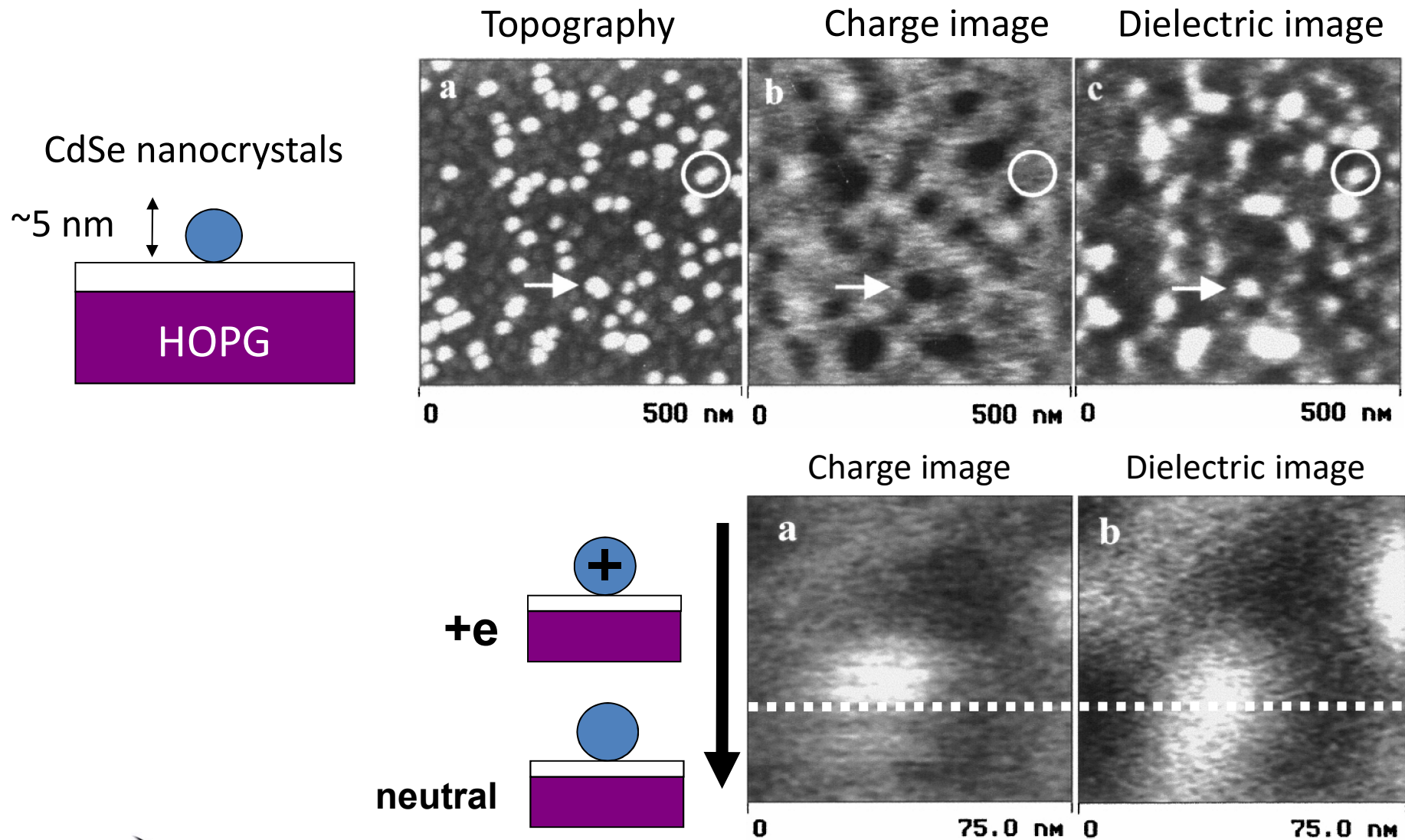
	in air	in vacuum, 300K	vacuum, 1-5 K
	limited by thermal noise		deflection noise, thermal noise, ...
F'_{\min}	<p>$\sim 10^{-5}$ N/m</p> <p>B=100Hz, Q=200 A=25nm</p>	<p>a few 10^{-6} N/m</p> <p>B=50Hz, Q=20000 A=15nm</p>	<p>$\sim 10^{-3}$ N/m</p> <p>B=25Hz, Q=20000 A=200pm</p>
$\langle z \rangle$	50-100nm	10-20nm	< 1 nm

Long-range (LR)

LR + SR

Short-range (SR)

Resolution : single charge detection in ambient air ?



Time resolution

- In general, limited by the phase demodulation of the cantilever oscillation
- better resolution possible :
 - fast frequency shift demodulation,
 - oscillation transients (sub- μ s see D. Ginger et al. Nanoletters 2012)
 - response under modulated illumination (see Ł. Borowik)

Quantitative charge measurements ?

- in general, semi-quantitative models only
- difficult due to the large variety of dielectric environments
- numerical simulations in most situations
- single charge events as calibration



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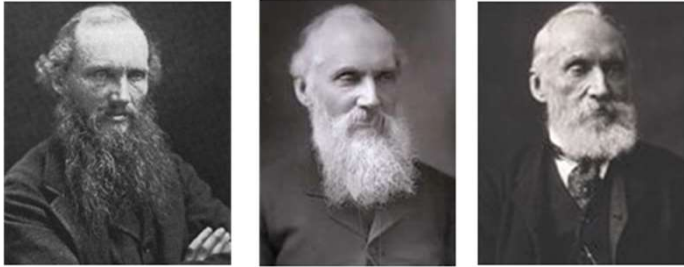
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Principle ...

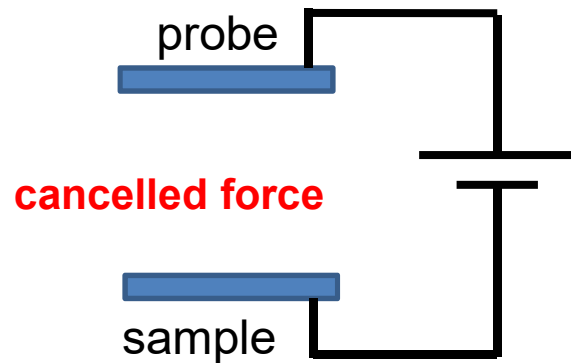
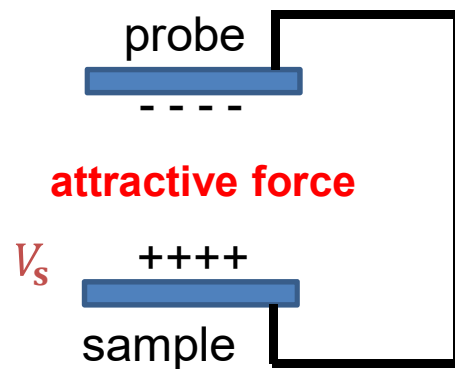


Measuring surface potentials from forces

- Lord Kelvin (1898)
- Zisman (1932) : vibrating Kelvin probe (down to mm size)
- Nonnenmacher (1991) : Kelvin probe **force** microscopy

different metals

e.g. $\phi_{\text{probe}} > \phi_{\text{sample}}$

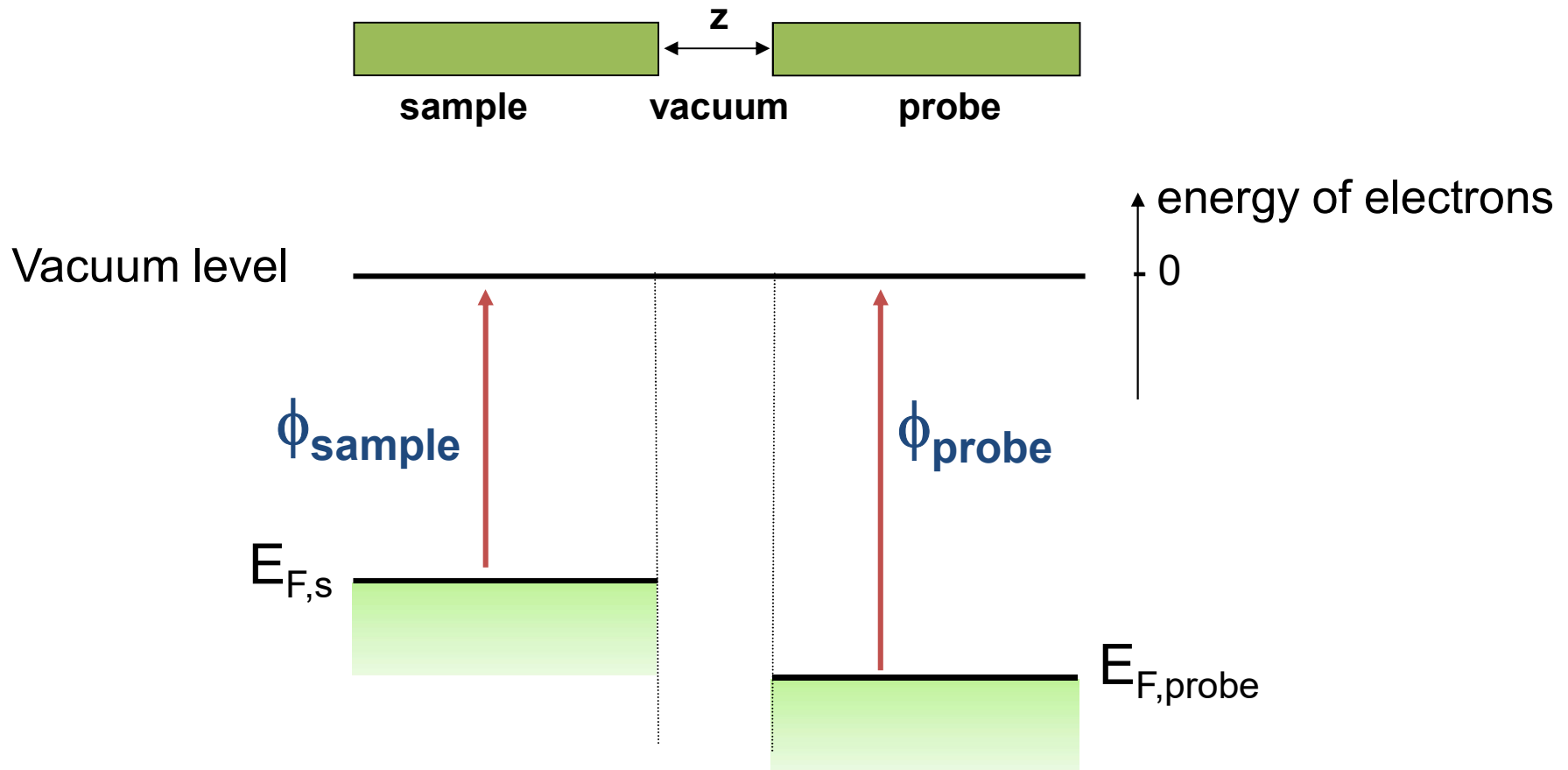


$$V_{DC} = \frac{\phi_{\text{probe}} - \phi_{\text{sample}}}{|e|}$$

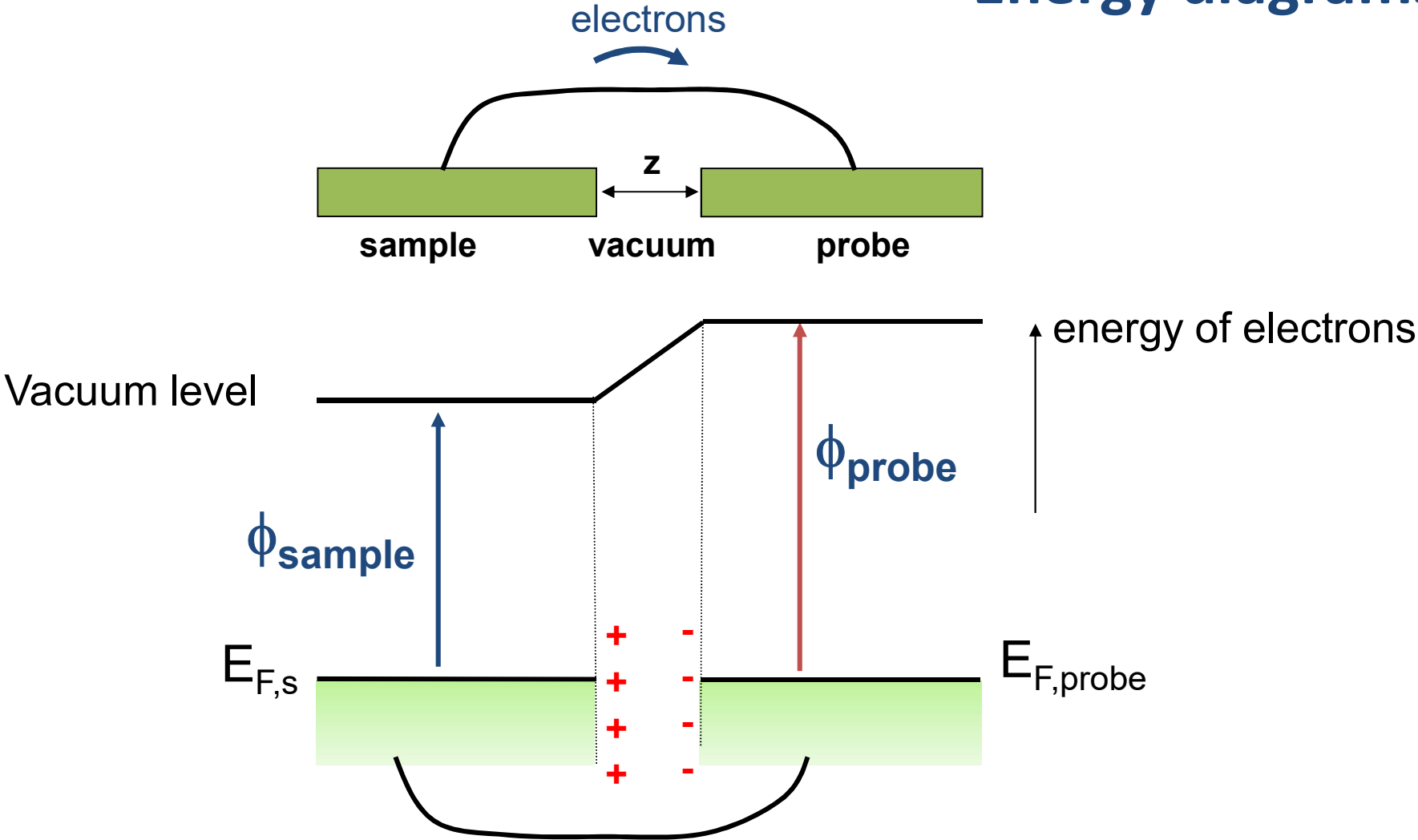
V_{CPD} ou V_s

Work function
measurement

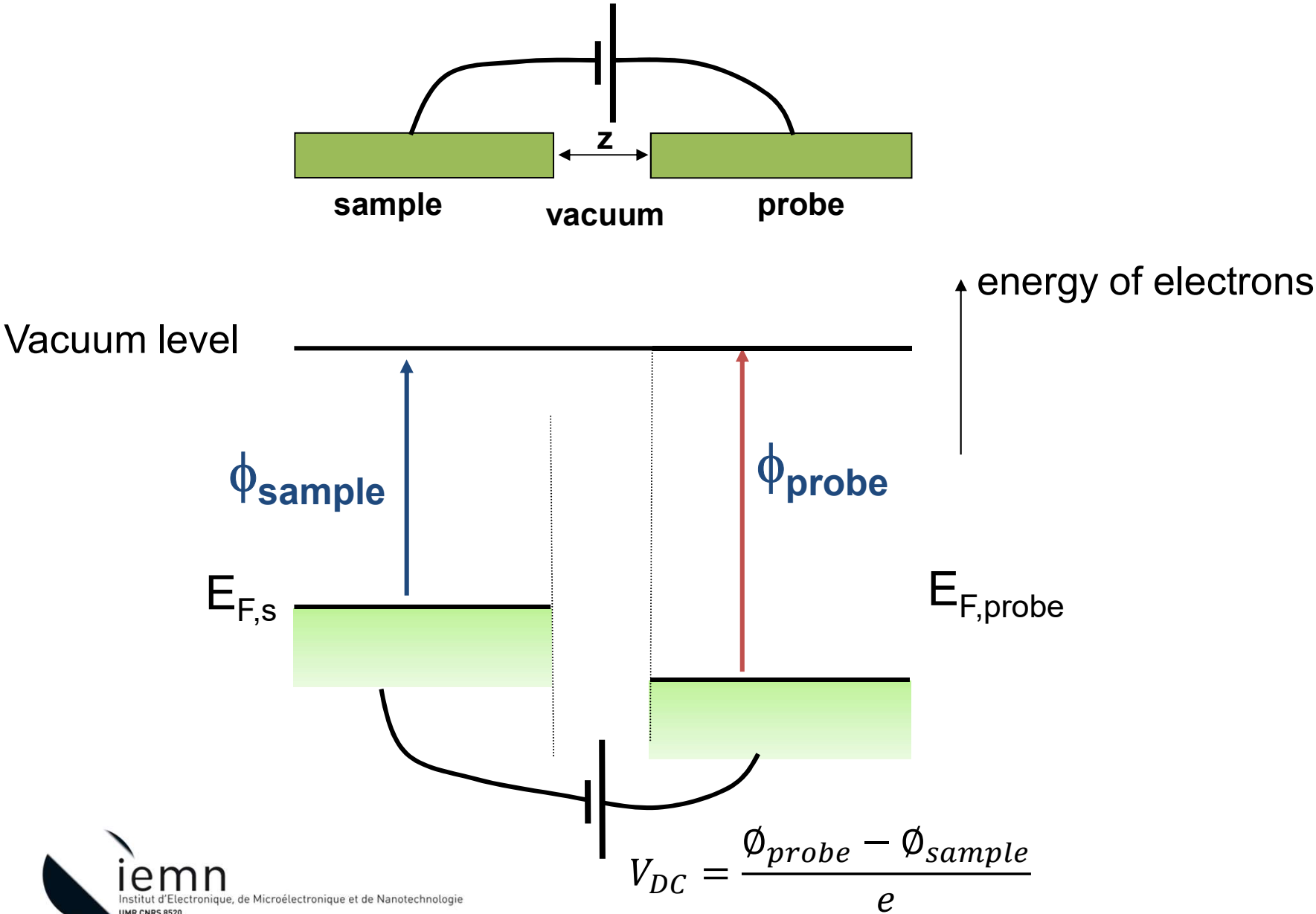
Energy diagrams



Energy diagrams



Energy diagrams



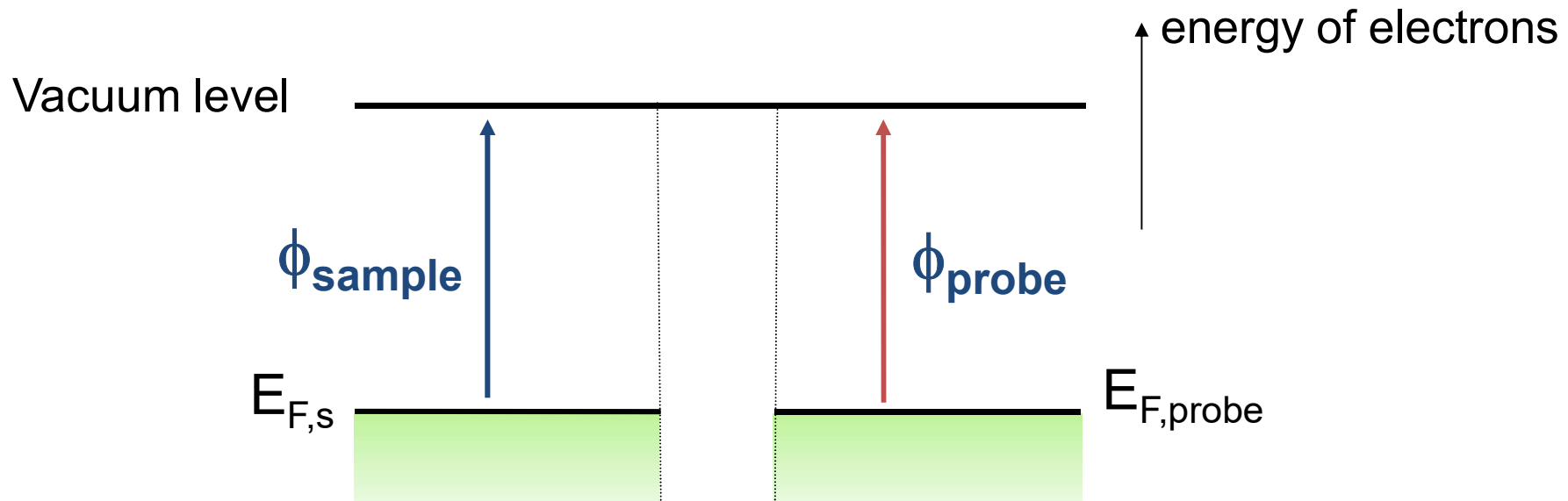
A few remarks ...

- The sign of V_{dc} is user-dependent (V_{dc} at the tip, or at the sample)
- V_{dc} at the tip (and V_s at the surface)
 - ‘electrostatics-friendly’ convention :
a positive charge or dipole (e.g. adsorbate) is ‘seen’ as a positive V_s

A few remarks ...

- The sign of V_{dc} is user-dependent (V_{dc} at the tip, or at the sample)
- V_{dc} at the tip (and V_s at the surface)

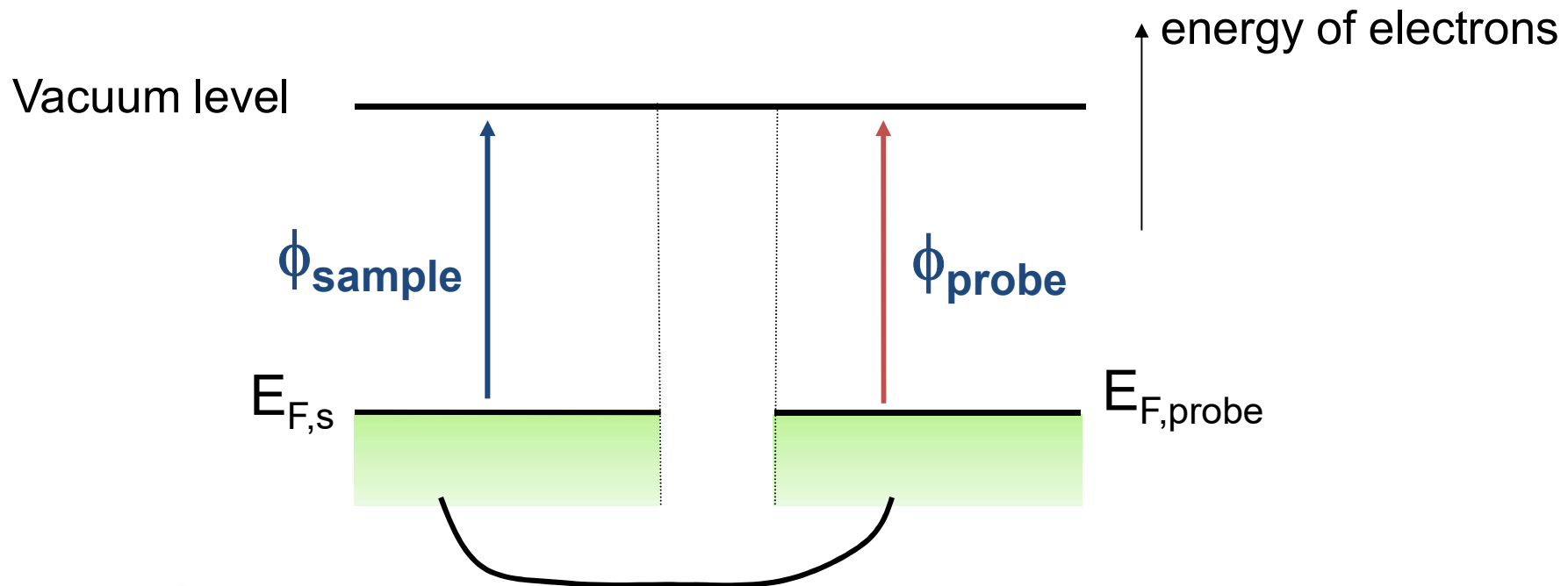
‘electrostatics-friendly’ convention :
a positive charge or dipole (e.g. adsorbate) is ‘seen’ as a positive V_s



A few remarks ...

- The sign of V_{dc} is user-dependent (V_{dc} at the tip, or at the sample)
- V_{dc} at the tip (and V_s at the surface)

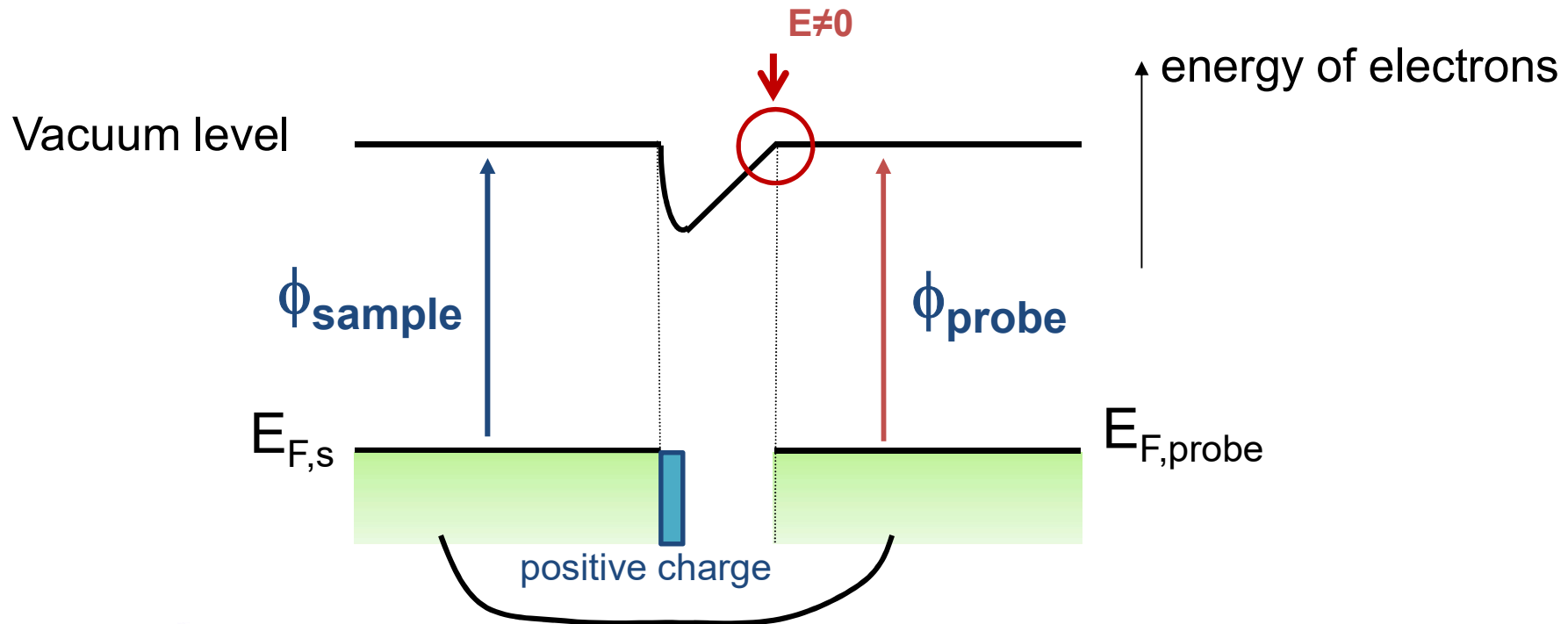
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A few remarks ...

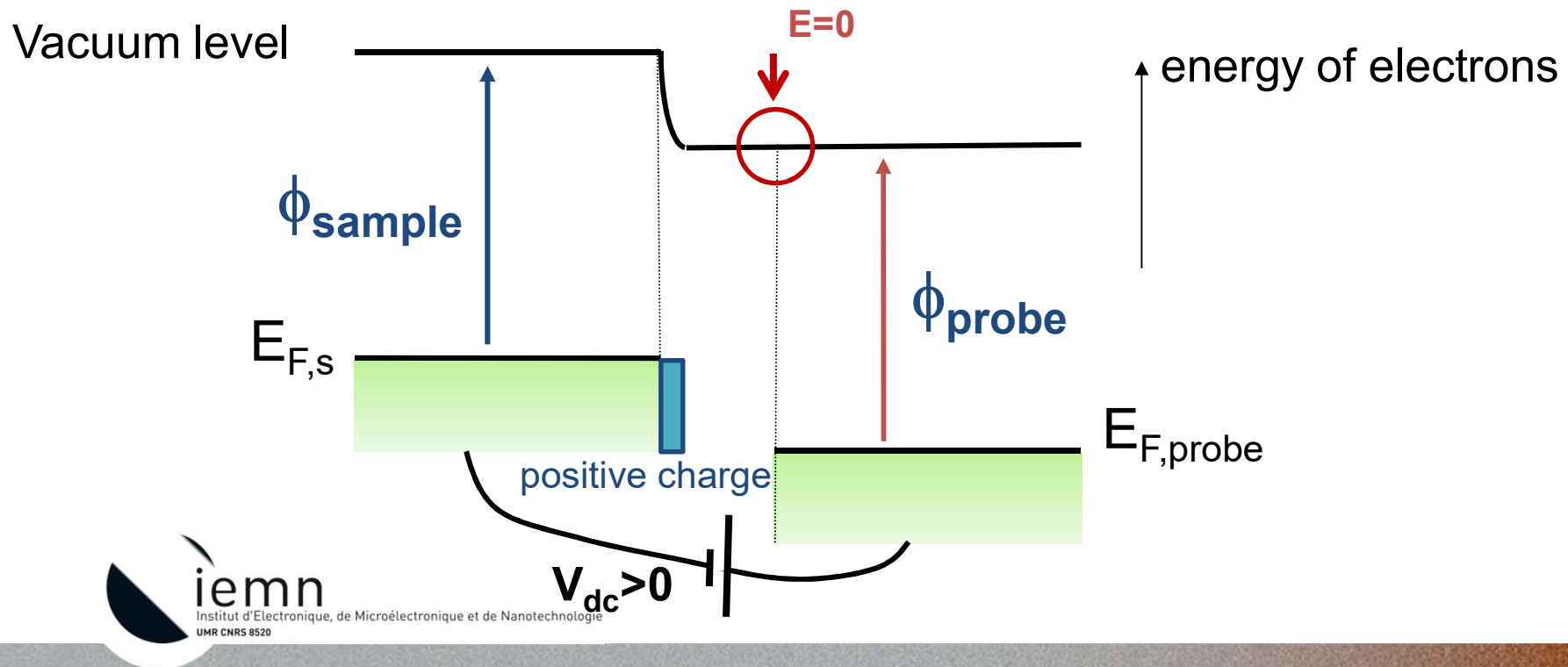
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A few remarks ...

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- **V_{dc} at the tip** (and V_s at the surface)
‘electrostatics friendly’ convention
a positive charge or dipole (e.g. adsorbate) is ‘seen’ as a positive V_s
- **V_{dc} at the sample**
‘work-function friendly’ convention :
a material with a larger work-function will be imaged as « more positive »
in KPFM images

A NEW METHOD OF MEASURING CONTACT POTENTIAL DIFFERENCES IN METALS

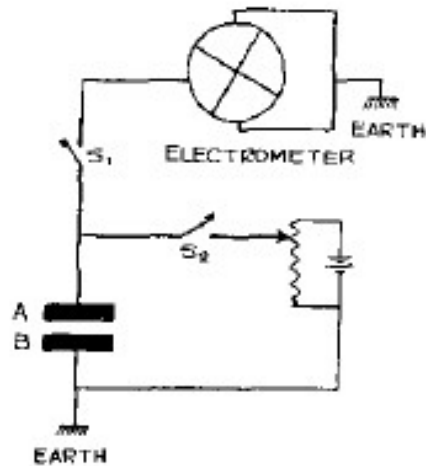
By W. A. ZISMAN

[JEFFERSON PHYSICAL LABORATORY, HARVARD UNIVERSITY, CAMBRIDGE, MASS.

RECEIVED MARCH 5, 1932]

ABSTRACT

A new method is described for measuring the contact potential differences between dissimilar metals. It enables one to measure the p.d. to 1/1000 volt in a few seconds of manipulation. An apparatus is described for studying metals in air and another is described for high vacuum work.

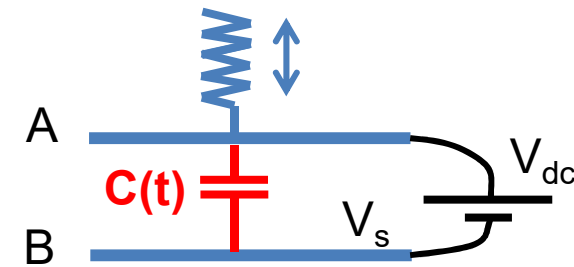


Kelvin method

Response of the electrometer deflection as a function of V_{dc} to find the zero force

Zisman method

Rev. Sci. Instrum. 3, 367 (1932)



$$C = C_0 + \Delta C \cdot \sin \omega t$$



$$i(t) = \Delta C \cdot \omega \cdot [V_{dc} - V_s] \cdot \cos(\omega t)$$



to a loud speaker (!)
 $(\omega$ in the audio range) :
 zero sound for $V_{dc} = V_s$



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Détection de charge(s) ?

Microscopie à sonde de Kelvin (KFM)

Modulation d'Amplitude (AM) vs Modulation de Fréquence (FM)

Effet des capacités latérales

Acquisition en boucle ouverte (OL-KFM)

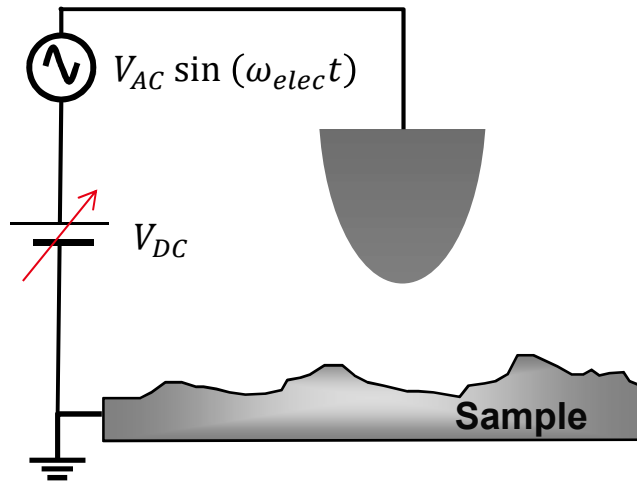
KFM & DFRT (Dual Frequency Resonant Tracking)

Travail de sortie : mesure quantitative ?

KFM en modulation d'amplitude (AM-KFM)

$$V = V_{DC} - V_{CPD} + V_{AC} \sin(\omega_{elec} t)$$

Force électrostatique
(3 composantes)



$$F_0 = \frac{1}{2} \frac{\partial C}{\partial z} \left[(V_{DC} - V_{CPD})^2 + \frac{V_{AC}^2}{2} \right]$$

$$F_{z, \omega_{elec}} = \frac{\partial C}{\partial z} (V_{DC} - V_{CPD}) V_{AC}$$

$$F_{z, 2 \omega_{elec}} = -\frac{1}{4} \frac{\partial C}{\partial z} V_{AC}^2$$

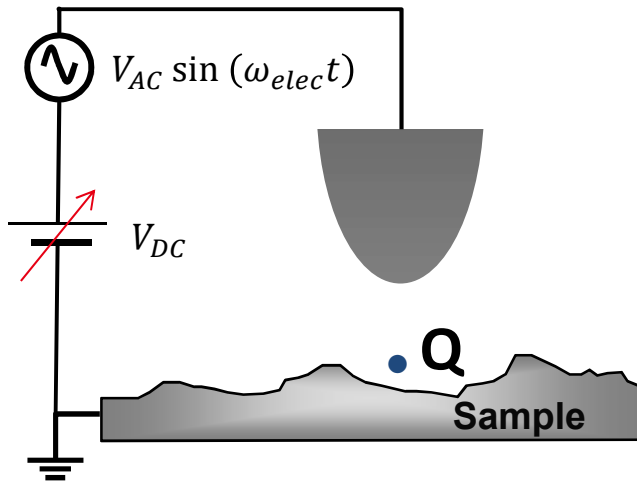
AM-KFM → **Annulation** de la composante à ω_{elec} de la force électrostatique

$$V_{DC} = V_{CPD}$$

KFM en modulation d'amplitude (AM-KFM)

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Force électrostatique (3 composantes)



$$F_0 = \frac{1}{2} \frac{\partial C}{\partial z} \left[(V_{DC} - V_{CPD})^2 + \frac{V_{AC}^2}{2} \right] + \text{contributions force image}$$

$$F_{z, \omega_{elec}} = \frac{\partial C}{\partial z} (V_{DC} - V_{CPD}) V_{AC} + K(z) Q V_{AC}$$

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AM-KFM → **Annulation** de la composante à ω_{elec} de la force électrostatique

$$V_{DC} = V_{CPD} + V_Q(z)$$

Simple passage

Excitation mécanique à la résonance du levier ($f_{méca} = f_0$)

Tapping (Air)
ou
nc-AFM (Vide, UHV)



Modulation électrique à la 1^{ère} harmonique ($f_{élec} = f_1 \approx 6,3 \times f_0$)

Démodulation à $f_{élec} \rightarrow$ amplitude

Double passage

1^{er} passage

Excitation mécanique à la résonance du levier ($f_{méca} = f_0$)

Tapping (Air)
ou
nc-AFM (Vide, UHV)

2^{ème} passage : lift

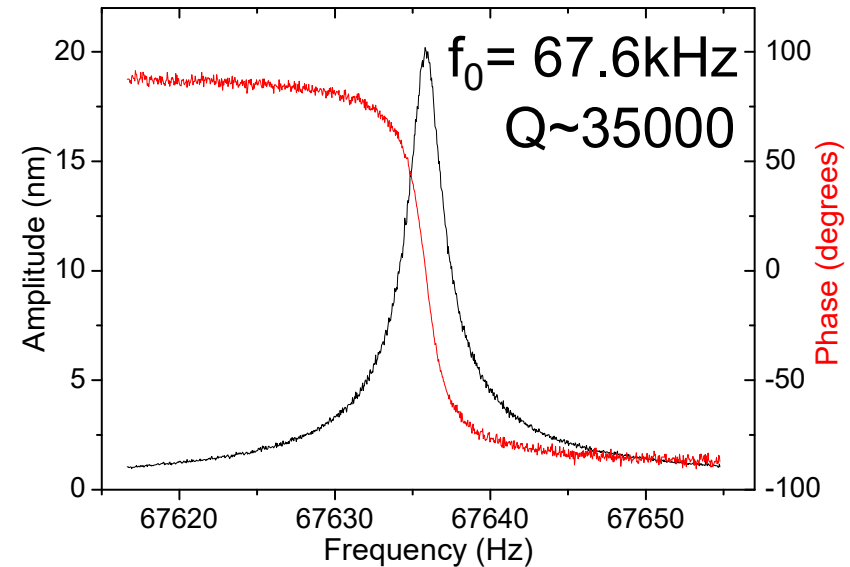
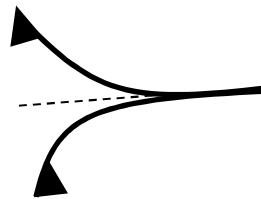
Modulation électrique à la résonance du levier ($f_{élec} = f_0$)

Démodulation à $f_{élec} \rightarrow$ amplitude
Hauteur de lift (20 à 100 nm)

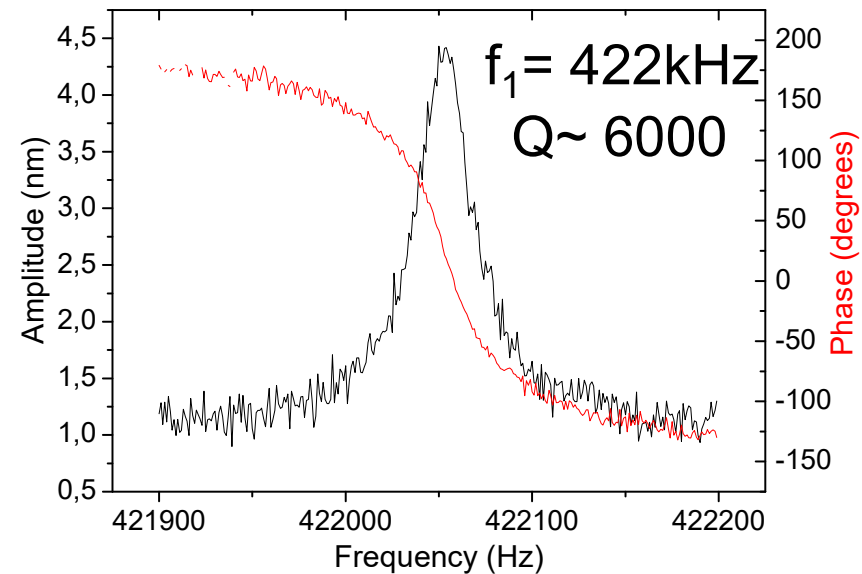
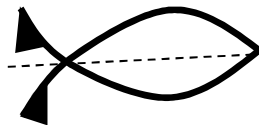
Example of a single-pass (UHV) AM-KPFM mode

- first resonance f_0
- mechanical excitation
- non-contact AFM

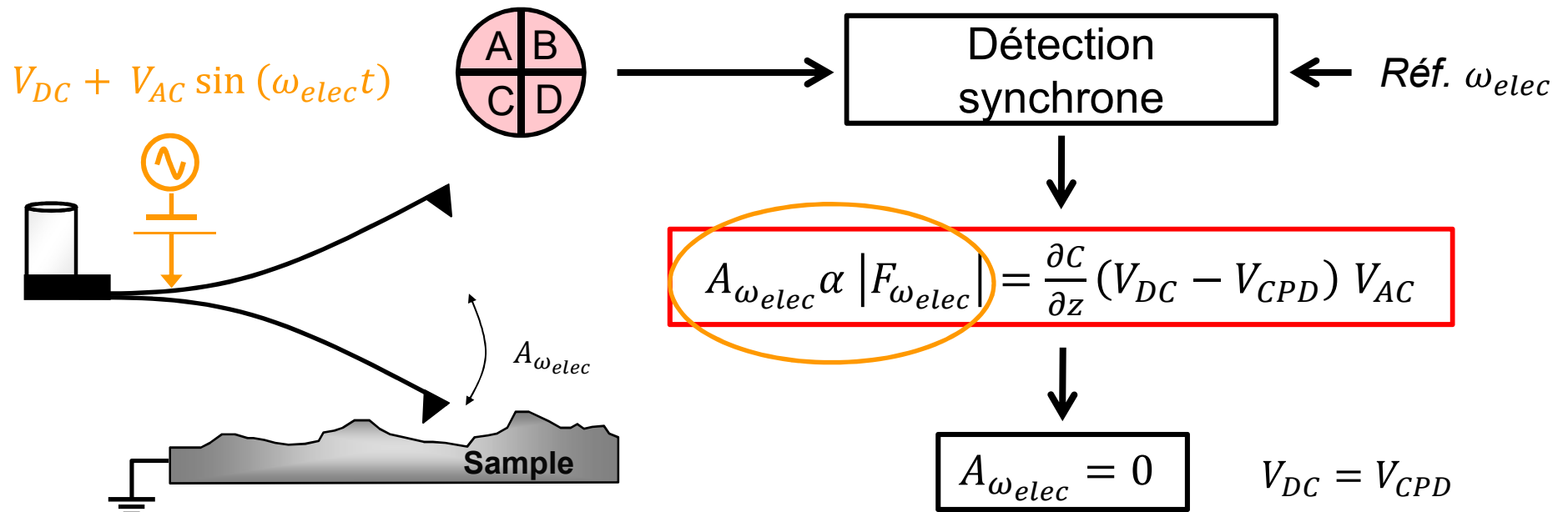
$\Delta f = -5\text{Hz}$ oscillation amplitude 15 nm
minimum tip-substrate distance $\sim 5\text{nm}$



- second resonance $f_1 \sim 6.2 \times f_0$
- electrostatic excitation
- KFM loop at f_1



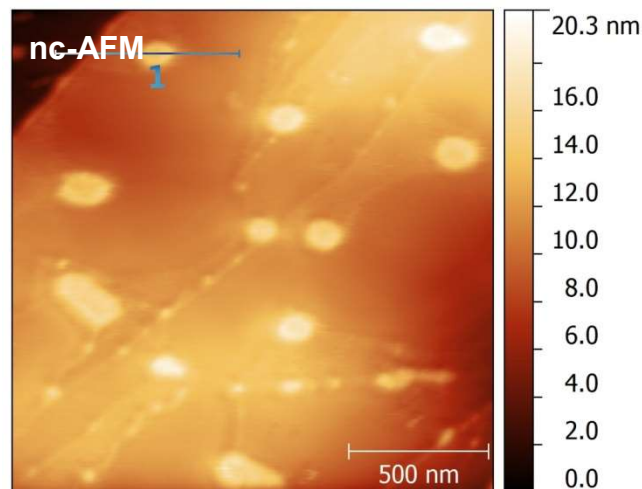
AM-KFM : EN PRATIQUE



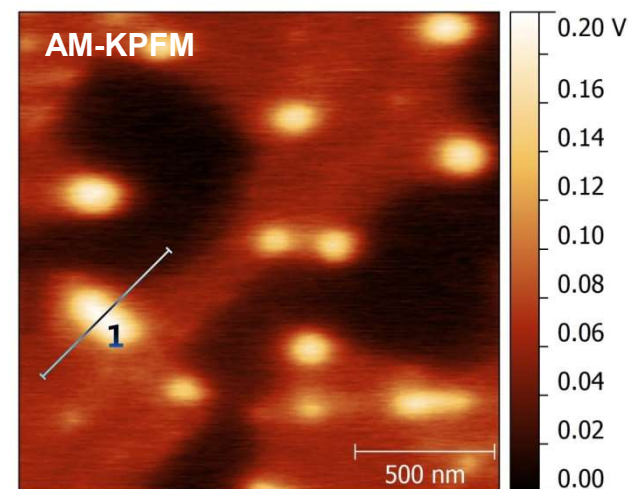
- Une boucle de contre-réaction (PID) annule la composante $A_{\omega_{elec}}$ en ajustant la valeur du V_{DC}

Imaging ...

Doped nanocrystals inducing charge transfers to the substrate



topo : $A_{pp} = 20 \text{ nm}$, $\Delta f = -5 \text{ Hz}$;
 $1,7 \mu\text{m} * 1,7 \mu\text{m}$; $512 * 512$ pixels;
tip-sample distance of 4-6 nm

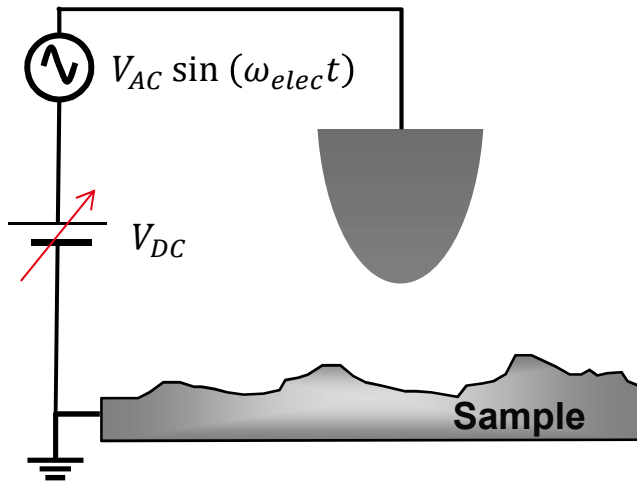


AM-KPFM : $V_{ac} = 200 \text{ mV}$;
 $V_{dc} = 2 \text{ V}$; $\tau = 100 \mu\text{s}$

KFM en modulation de fréquence (FM-KFM)

$$V = V_{DC} - V_{CPD} + V_{AC} \sin(\omega_{elec} t)$$

Gradient de force électrostatique (3 composantes)



$$\frac{\partial F_{z,0}}{\partial z} = \frac{1}{2} \frac{\partial^2 C}{\partial z^2} \left[(V_{DC} - V_{CPD})^2 + \frac{V_{AC}^2}{2} \right]$$

$$\frac{\partial F_{z,\omega_{elec}}}{\partial z} = \frac{\partial^2 C}{\partial z^2} (V_{DC} - V_{CPD}) V_{AC}$$

$$\frac{\partial F_{z,2\omega_{elec}}}{\partial z} = -\frac{1}{4} \frac{\partial^2 C}{\partial z^2} V_{AC}^2$$

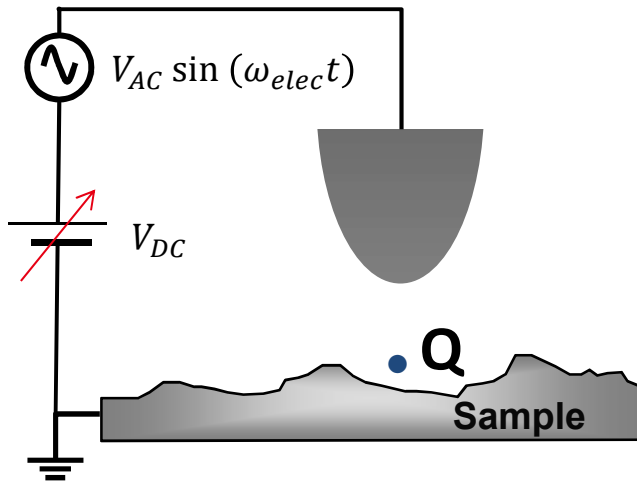
FM-KFM → **Annulation** de la composante à ω_{elec} du gradient de la force électrostatique

$$V_{DC} = V_{CPD}$$

KFM en modulation de fréquence (FM-KFM)

$$V = V_{DC} - V_{CPD} + V_{AC} \sin(\omega_{elec} t)$$

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Simple passage

Excitation mécanique à la résonance du
levier ($f_{méca} = f_0$)

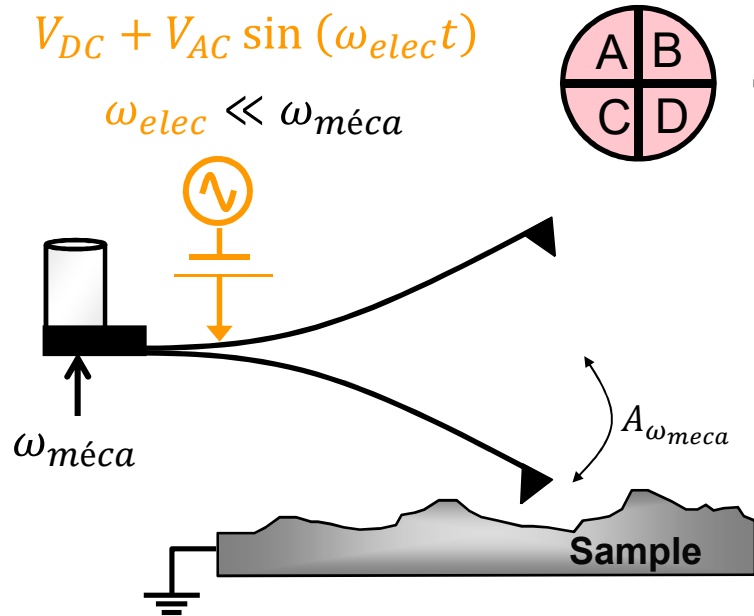
Tapping (Air)
ou
nc-AFM (Vide, UHV)



Modulation électrique à basse fréquence
($f_{élec} \ll f_0$)

Démodulation à $f_{élec}$ du signal de phase
mécanique (mode Tapping) ou du décalage de
fréquence (mode nc-AFM)

FM-KFM : EN MODE TAPPING (AIR)



Détection synchrone

← Réf. ω_{meca}

$$\Delta\varphi_{meca} = -\frac{Q}{k} \frac{\partial F}{\partial z} \propto \frac{\partial F_{elec}}{\partial z}$$

Modulation de fréquence

Détection synchrone

← Réf. ω_{elec}

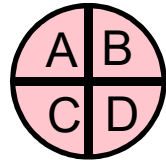
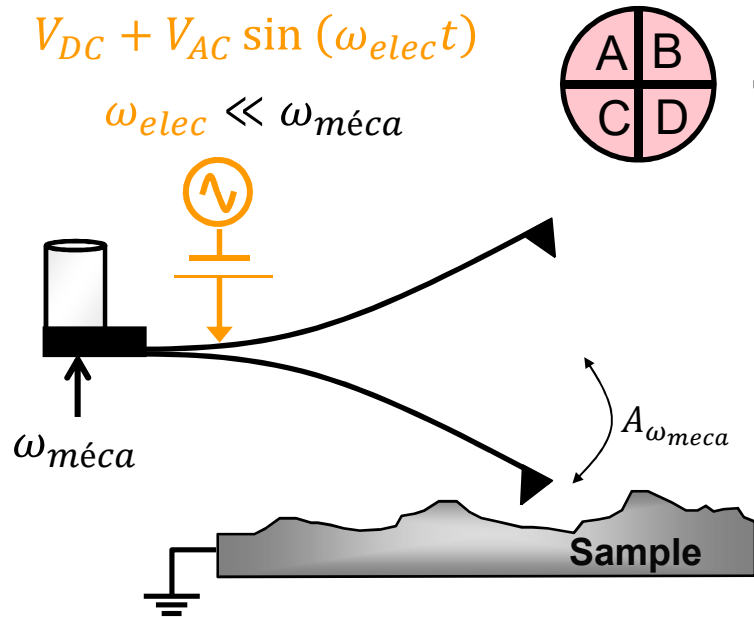
$$\left| \frac{\partial F_{\omega_{elec}}}{\partial z} \right| = \frac{\partial^2 C}{\partial z^2} (V_{DC} - V_{CPD}) V_{AC}$$

$$\left| \frac{\partial F_{\omega_{elec}}}{\partial z} \right| = 0$$

$$V_{DC} = V_{CPD}$$

- Une boucle de contre-réaction (PID) annule la composante $\frac{\partial F_{\omega_{elec}}}{\partial z}$ en ajustant la valeur du V_{DC}

FM-KFM : EN MODE NC-AFM (UHV)



$$\Delta f_{meca} = - \frac{1}{2k} \frac{\partial F}{\partial z} \propto \frac{\partial F_{elec}}{\partial z}$$

Modulation de fréquence



Réf. ω_{elec}

$$\left| \frac{\partial F_{\omega_{elec}}}{\partial z} \right| = \frac{\partial^2 C}{\partial z^2} (V_{DC} - V_{CPD}) V_{AC}$$

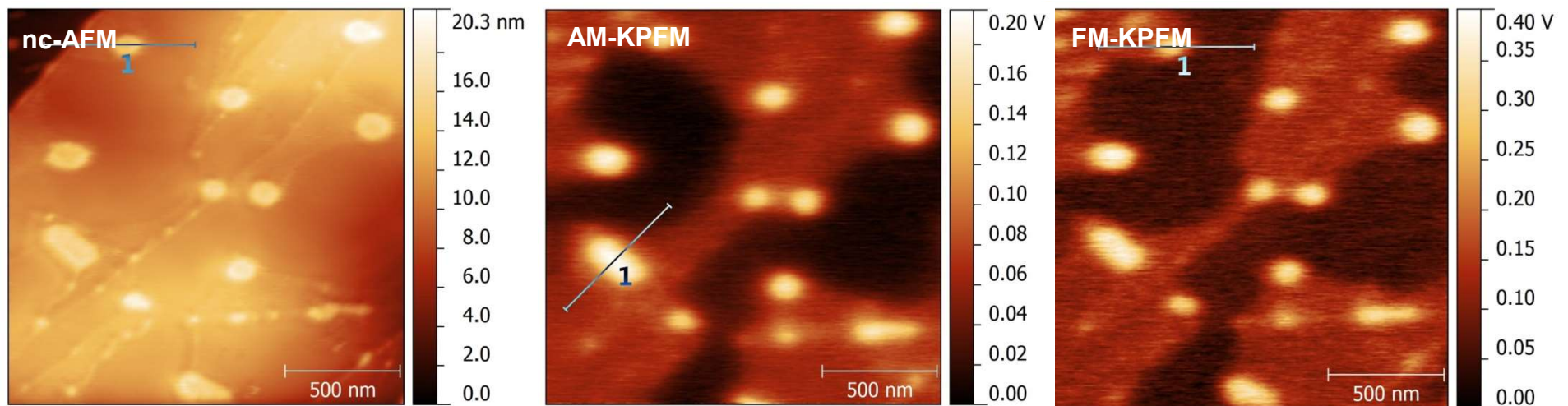
$$\left| \frac{\partial F_{\omega_{elec}}}{\partial z} \right| = 0$$

$$V_{DC} = V_{CPD}$$

AM-KPFM versus FM-KPFM

Imaging ...

Doped nanocrystals inducing charge transfers to the substrate



topo : $A_{pp} = 20 \text{ nm}$, $\Delta f = -5 \text{ Hz}$;
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tip-sample distance of 4-6 nm

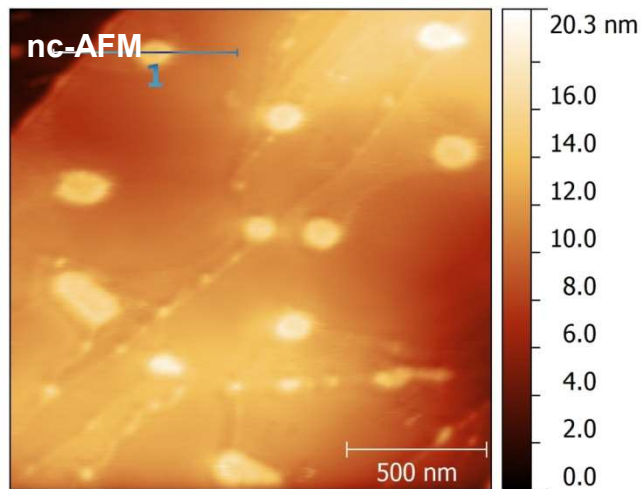
AM-KPFM : $V_{ac} = 200 \text{ mV}$; $V_{dc} = 2 \text{ V}$; $\tau = 100 \mu\text{s}$

FM-KPFM : $f_{ac} \sim 50\text{Hz}$; $V_{ac} = 200 \text{ mV}$

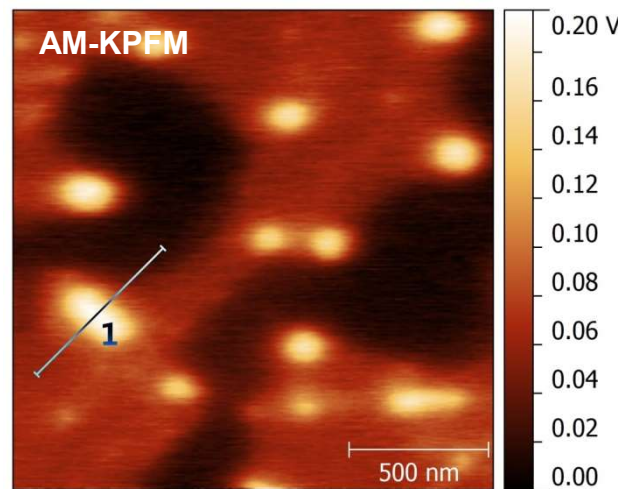
AM-KPFM versus FM-KPFM

	signal to noise	resolution
AM-KPFM	+	-
FM-KPFM	-	+

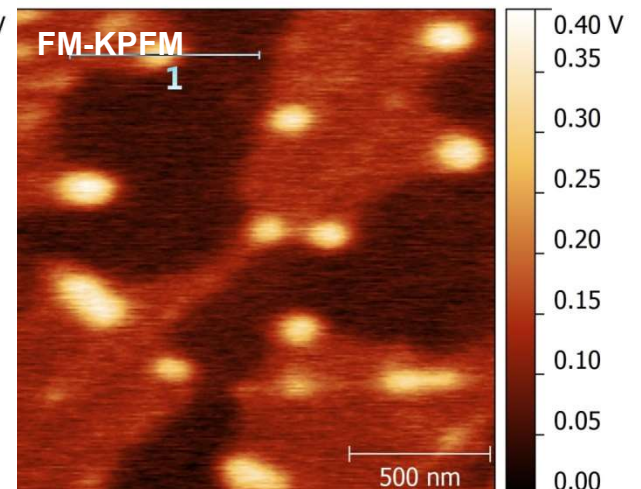
- less ac cross-talk
- no need for a 2nd resonance



topo : $A_{pp} = 20 \text{ nm}$, $\Delta f = -5 \text{ Hz}$;
 $1,7 \mu\text{m} * 1,7 \mu\text{m}$; $512 * 512$ pixels;
 tip-sample distance of 4-6 nm



AM-KPFM : $V_{ac} = 200 \text{ mV}$; $V_{dc} = 2 \text{ V}$; $\tau = 100 \mu\text{s}$



FM-KPFM : $f_{ac} \sim 50\text{Hz}$; $V_{ac} = 200 \text{ mV}$



EN RÉSUMÉ : AM vs FM KFM

Modulation d'amplitude (AM-KFM)	Modulation de fréquence (FM-KFM)
$F_{\omega_e} = 0 \Leftrightarrow V_{DC} = \mp V_{CPD}$	$\frac{\partial F_{\omega_e}}{\partial z} = 0 \Leftrightarrow V_{DC} = \mp V_{CPD}$

Configurations

	Simple passage		Double passage
	AM-KFM	FM-KFM	AM-KFM
Topographie	Tapping (air) ou non-contact (ultra-vide) : $f_{méca} = f_0$		
Modulation électrique	$f_1 \approx 6,3 \times f_0$ ou hors-résonance	$f_1 \ll f_0$	f_0 ou $f_1 \approx 6,3 \times f_0$ ou hors-résonance



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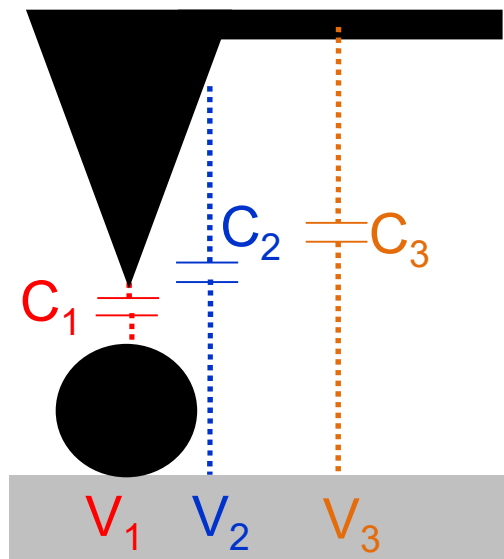
Effet des capacités latérales

Acquisition en boucle ouverte (OL-KFM)

KFM & DFRT (Dual Frequency Resonant Tracking ou ac-EFM)

Travail de sortie : mesure quantitative ?

Side-capacitance effects in AM- and FM-KPFM – 1/5



Nullification of the ω force component (AM-KPFM)

$$\frac{\partial C_1}{\partial z} (V_{DC} - V_1) V_{AC} + \frac{\partial C_2}{\partial z} (V_{DC} - V_2) V_{AC} + \frac{\partial C_3}{\partial z} (V_{DC} - V_3) V_{AC} = 0$$

$$V_{DC} = \frac{\frac{\partial C_1}{\partial z} V_1 + \frac{\partial C_2}{\partial z} V_2 + \frac{\partial C_3}{\partial z} V_3}{\frac{\partial C_1}{\partial z} + \frac{\partial C_2}{\partial z} + \frac{\partial C_3}{\partial z}}$$

KPFM : averaging technique

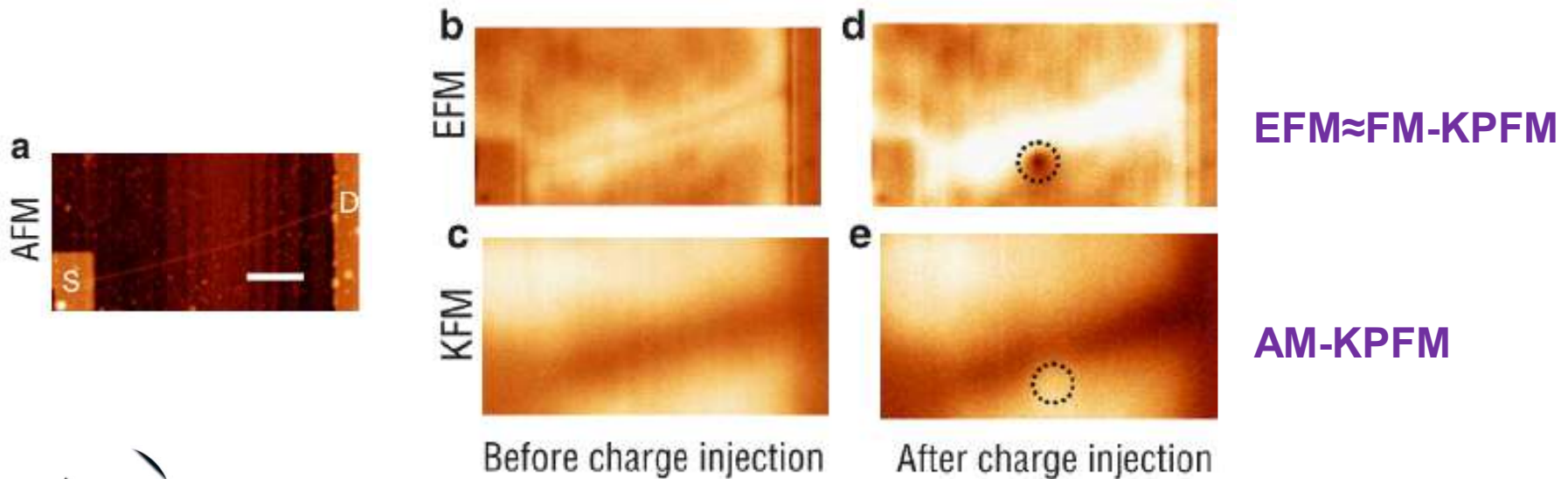
Side-capacitance effects in AM- and FM-KPFM - 2/5

generalization $\left\{ \begin{array}{l} \text{AM-KPFM} \\ \text{FM-KPFM} \end{array} \right.$

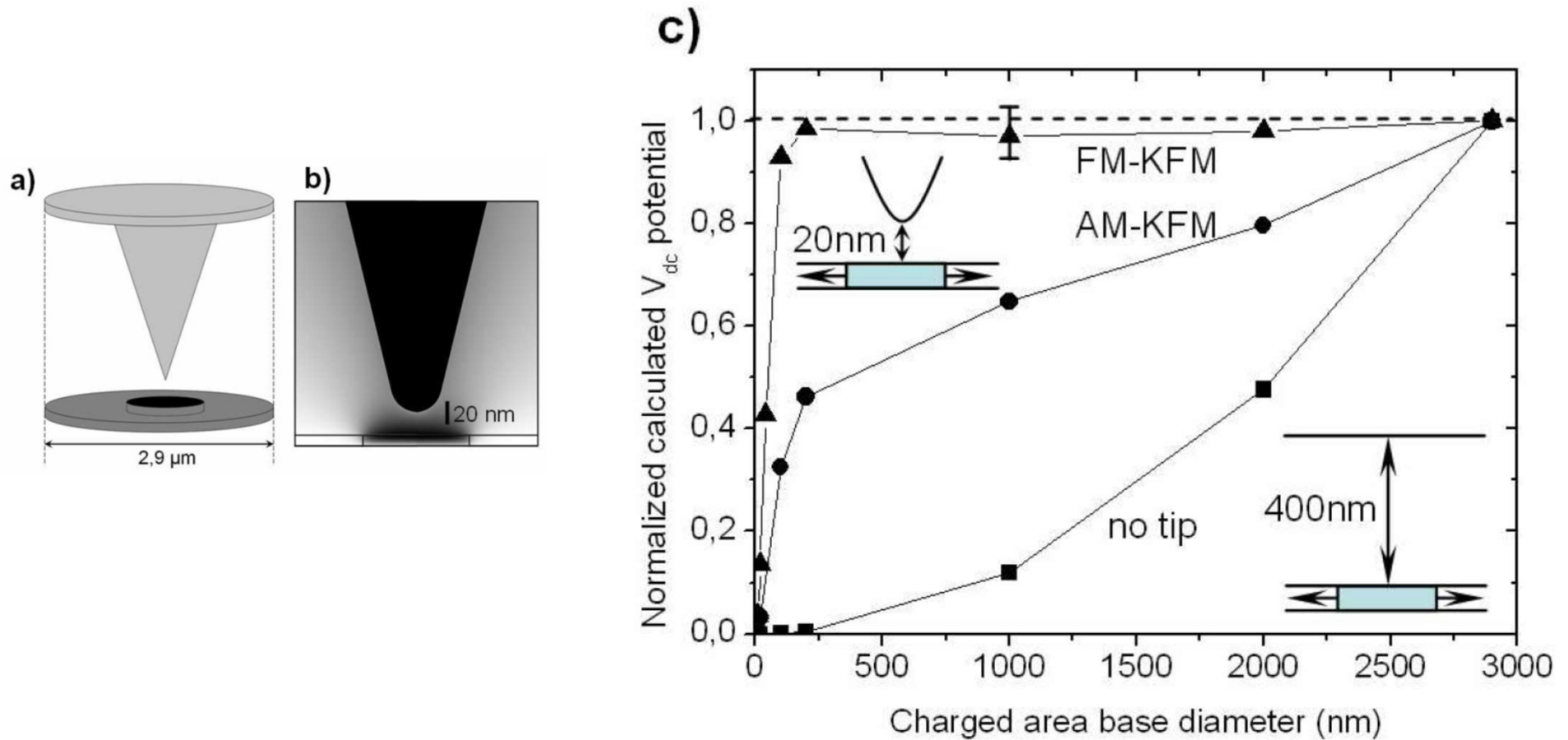
$$V_{DC} = \frac{\sum \frac{\partial C_i}{\partial z} V_i}{\sum \frac{\partial C_i}{\partial z}}$$

$$V_{DC} = \frac{\sum \frac{\partial^2 C_i}{\partial z^2} V_i}{\sum \frac{\partial^2 C_i}{\partial z^2}}$$

- intrinsic averaging effects in AM and FM modes
- dC_i/dz less 'peaked' at the tip than d^2C_i/dz^2 : less resolution in AM modes



Side-capacitance effects in AM- and FM-KPFM – 3/5

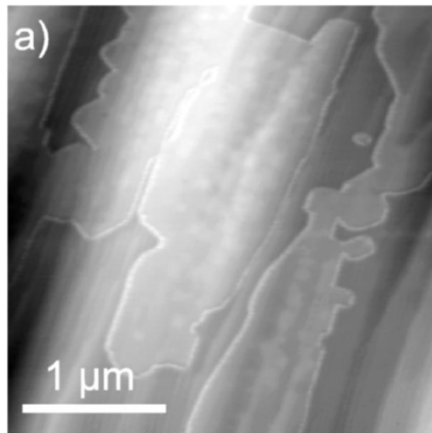


Both FM- and AM- modes are sensitive to side-capacitance effects at small size

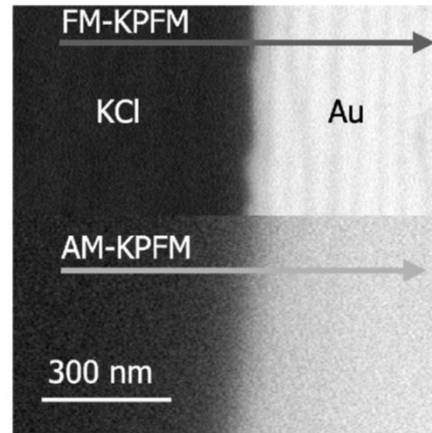
Side-capacitance effects in AM- and FM-KPFM – 4/5

	sensitivity	resolution
AM-KPFM	+	-
FM-KPFM	-	+

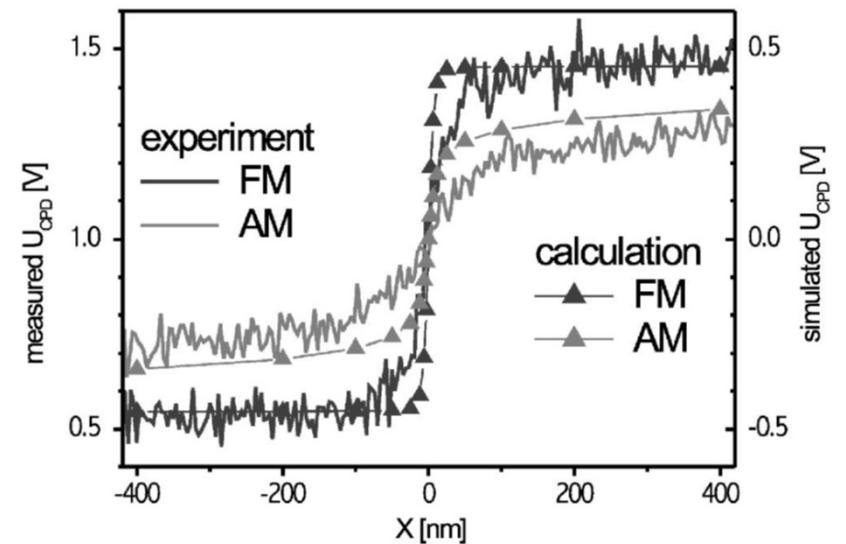
- less ac cross-talk
- no need for a 2nd resonance



KCl islands on Au 111
(topo)



KPFM across KCl island
boundaries



Side-capacitance effects in AM- and FM-KPFM – 5/5

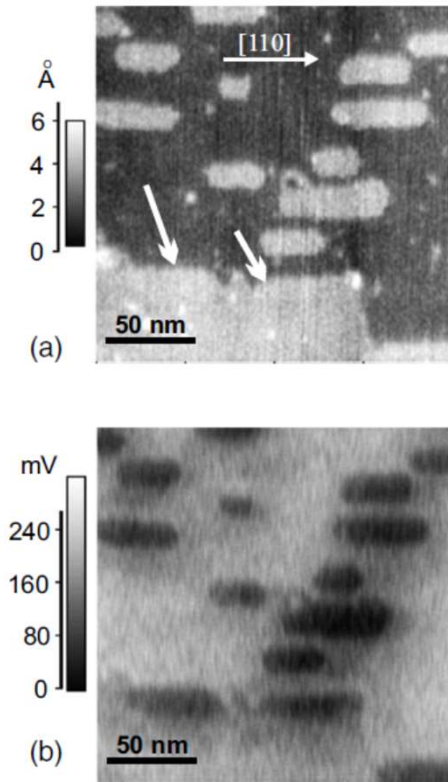
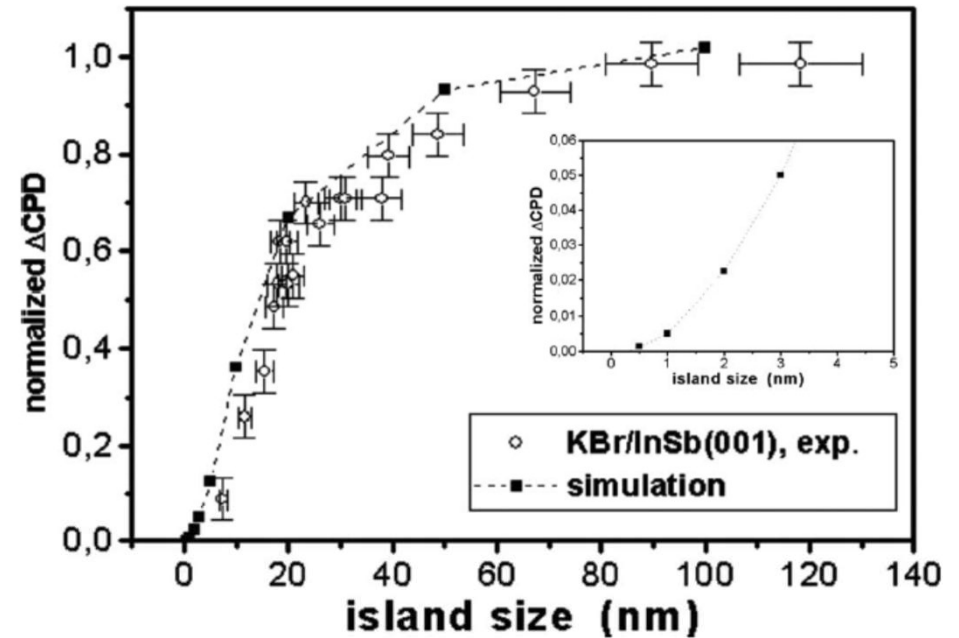


FIG. 1. (a) FM-KPFM topography and (b) Δ CPD images of KBr islands grown on InSb(001) surface ($f_0=111$, 1 kHz, $\Delta f = -17$ Hz). The white arrows indicate the KBr islands, which are topographically not resolved from the substrate terrace.



KBr on InSb(001)

FM-KPFM measurements

convolution in FM mode for structures with smaller size than the tip apex

F. Krok et al., Phys. Rev. B **77**, 235427 (2008)



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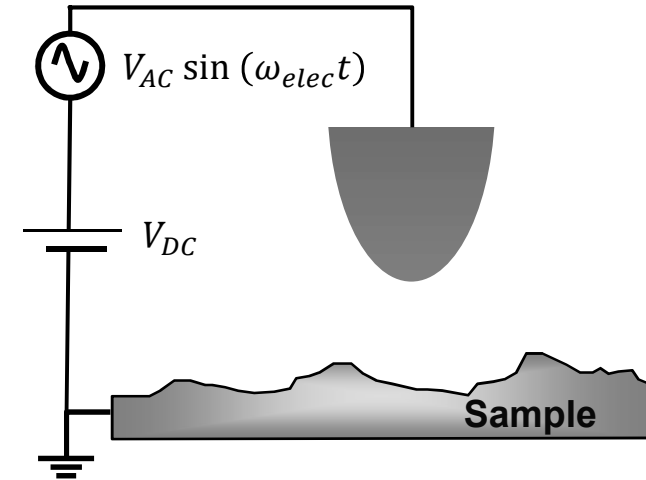
KFM & DFRT (Dual Frequency Resonant Tracking)

Travail de sortie : mesure quantitative ?

KFM en boucle ouverte (OL-KFM)

$$V = V_{DC} - V_{CPD} + V_{AC} \sin(\omega_{elec} t)$$

$$\omega_{elec} \ll \omega_0$$



Force électrostatique

Modulation d'Amplitude → AM-KFM sans boucle PID

$$F_{\omega_{elec}} = \frac{\partial C}{\partial z} (V_{DC} - V_{CPD}) V_{AC}$$

$$F_{2\omega_{elec}} = -\frac{1}{4} \frac{\partial C}{\partial z} V_{ac}^2$$



$$\frac{F_{\omega}}{F_{2\omega}} = -\frac{4}{V_{AC}} (V_{DC} - V_{CPD})$$

$$V_{CPD} = V_{DC} - \frac{F_{\omega} / F_{2\omega} \times V_{AC}}{4}$$

Simple passage

Excitation mécanique à la résonance du levier ($f_{méca} = f_0$)

Tapping (Air)
ou
nc-AFM (Vide, UHV)



Modulation électrique $f_{élec} \ll f_{méca}$

Démodulation à $f_{élec}$ et à $2 \times f_{élec} \rightarrow$
amplitudes correspondantes

Double passage

1^{er} passage

Excitation mécanique à la résonance du levier ($f_{méca} = f_0$)

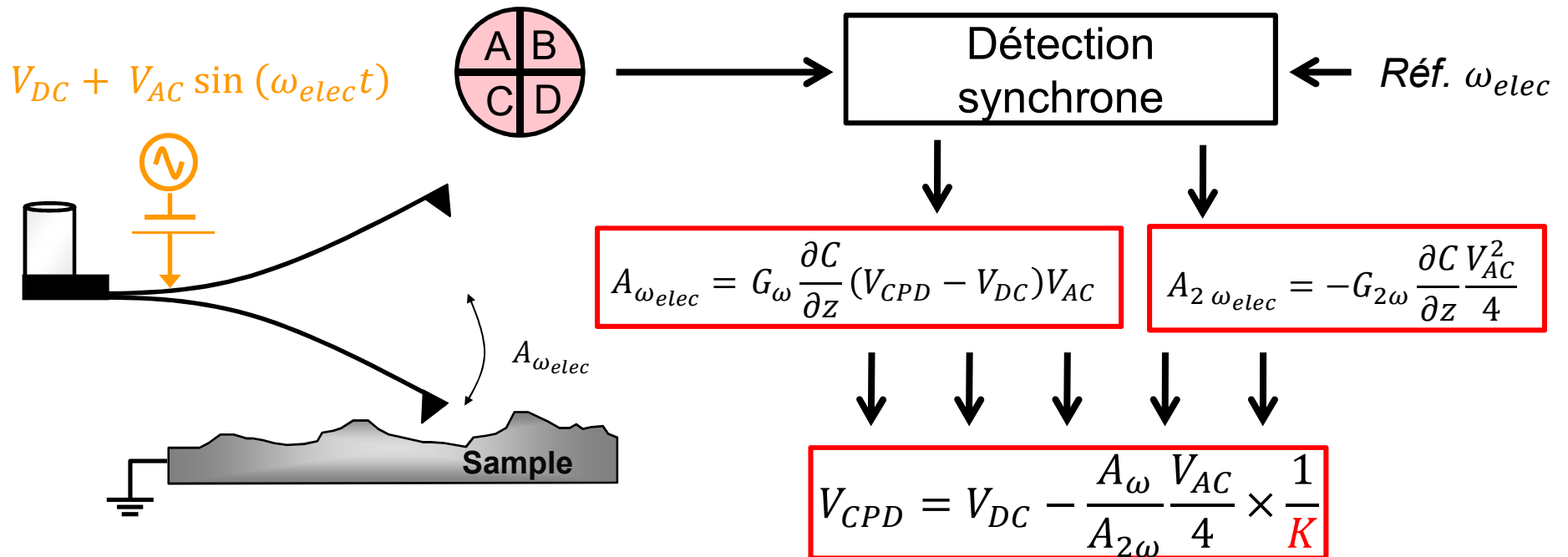
Tapping (Air)
ou
nc-AFM (Vide, UHV)

2^{ème} passage : lift

Modulation électrique $f_{élec} \ll f_{méca}$

Démodulation à $f_{élec}$ et à $2 \times f_{élec} \rightarrow$
amplitudes
Hauteur de lift (20 à 100 nm)

AM-KFM : EN PRATIQUE



- Calibration préalable de la valeur de K
- Calcul a posteriori du V_{CPD}

- Theory**

$$A_{\omega} = G_{\omega} \frac{\partial C}{\partial Z} (V_{CPD} - V_{DC}) V_{AC} > 0$$

$$A_{2\omega} = G_{2\omega} \frac{\partial C}{\partial Z} \frac{V_{AC}^2}{4} > 0$$

- Phase ajustement**

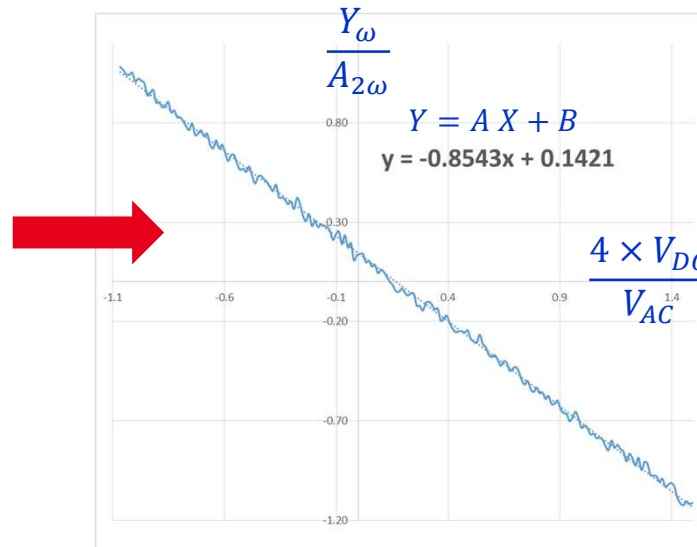
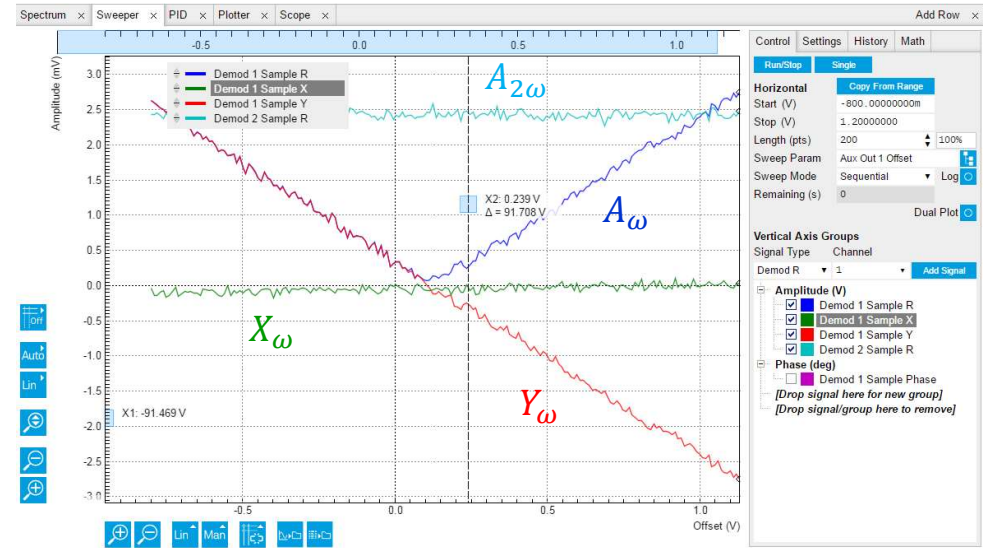
$$X_{\omega} = A_{\omega} \cos(\varphi) = 0$$

$$Y_{\omega} = A_{\omega} \sin(\varphi)$$

$$\frac{Y_{\omega}}{A_{2\omega}} = \frac{G_{\omega}}{G_{2\omega}} \frac{4}{V_{AC}} (V_{DC} - V_{CPD})$$

K_{gain}

$$V_{CPD} = V_{DC} - \frac{Y_{\omega}}{A_{2\omega}} \times K_{gain} \frac{V_{AC}}{4}$$



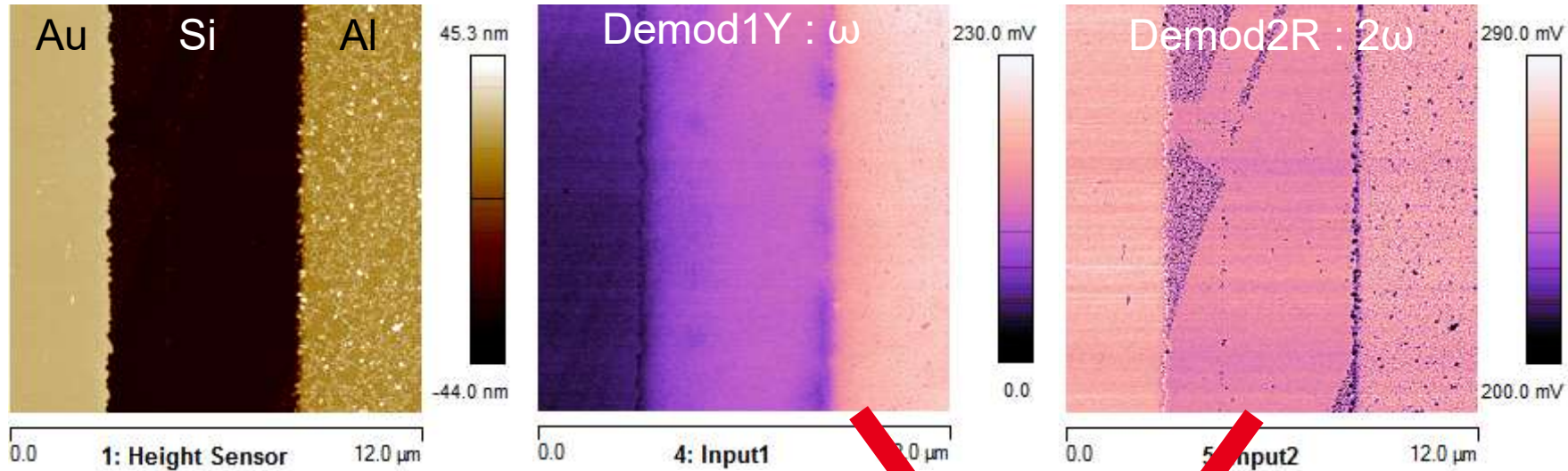
$$A = K_{gain} = -0.8543$$

$$B = -\frac{4K_{gain}V_{CPD}}{V_{AC}} = 0.1421$$

$$V_{CPD}(@0V) = 0.12 V$$

Mesure sur une couche d'Au
V_{ac}=3 V

EXAMPLE

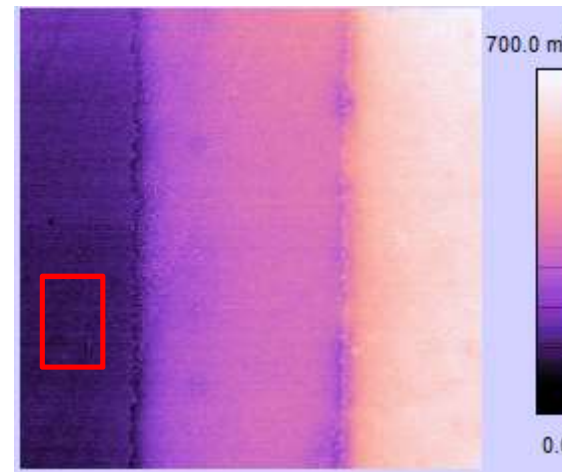


Calculated V_{CPD} (with Nanoscope Analysis)

$$V_{CPD} = \frac{V_{ac} Demod1Y}{4K Demod2R}$$

0,878

$$V_{CPD} = 0.13 V$$



Calculated V_{CPD}
 $V_{ac} = 3 V$
 $X_{gain} = -0.854$

OL-KFM en modulation de fréquence ?

Gradient de force électrostatique

FM-KFM sans boucle PID

$$\frac{\partial F_{z,\omega_{elec}}}{\partial z} = \frac{\partial^2 C}{\partial z^2} (V_{DC} - V_{CPD}) V_{AC}$$

$$\frac{\partial F_{z,2\omega_{elec}}}{\partial z} = -\frac{1}{4} \frac{\partial^2 C}{\partial z^2} V_{AC}^2$$



$$V_{CPD} = V_{DC} - \frac{F'_{\omega} / F'_{2\omega} \times V_{AC}}{4}$$

EFM modulé (ac-EFM)

Imagerie de charges et de prop. diélectriques

SOMMAIRE

Quelques rappels : force capacitive & CPD

Microscopie à force électrostatique (EFM)

Détection de charge(s) ?

Microscopie à sonde de Kelvin (KFM)

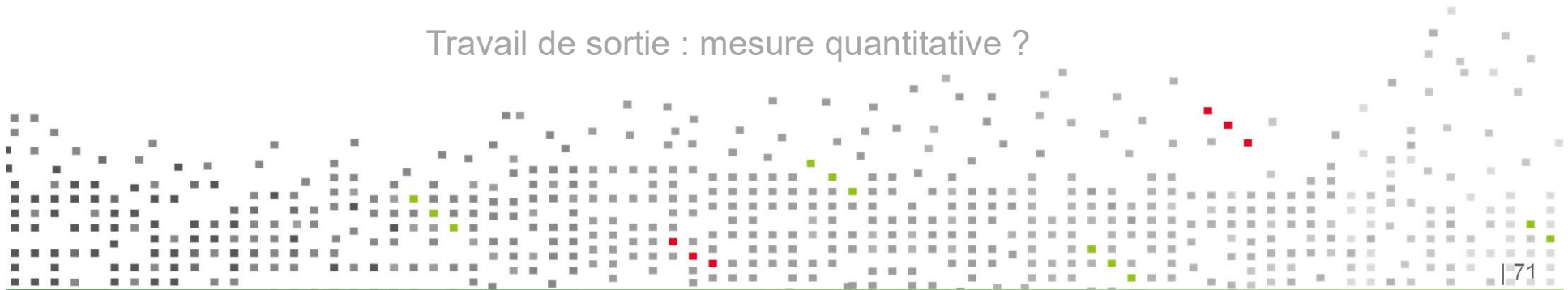
Modulation d'Amplitude (AM) vs Modulation de Fréquence (FM)

Effet des capacités latérales

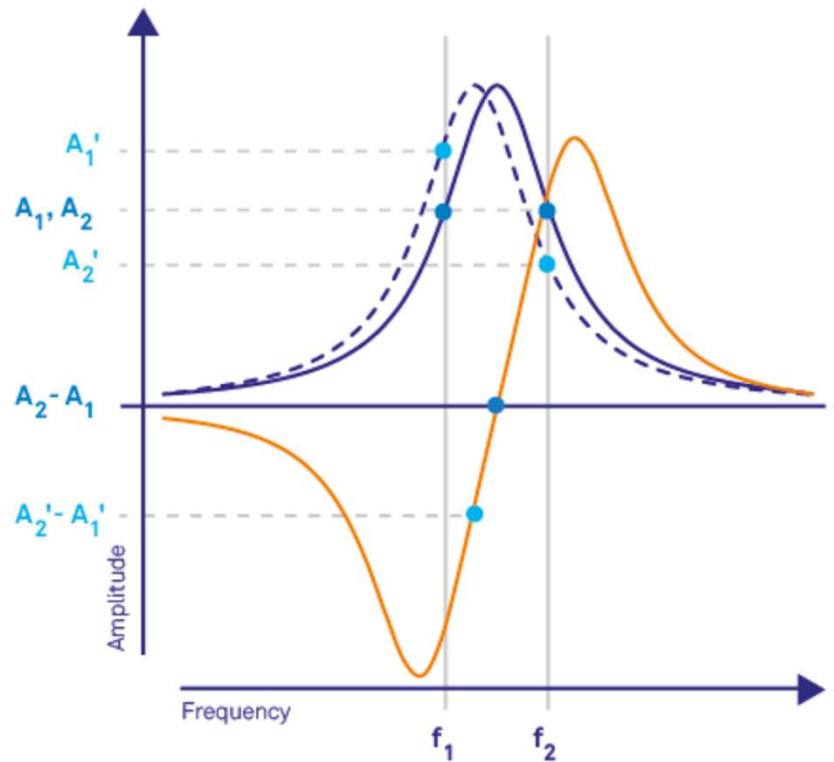
Acquisition en boucle ouverte (OL-KFM ou ac-EFM)

KFM & DFRT (Dual Frequency Resonant Tracking)

Travail de sortie : mesure quantitative ?



DUAL FREQUENCY RESONANT TRACKING (DFRT)



- **Méthode de suivi de fréquence**

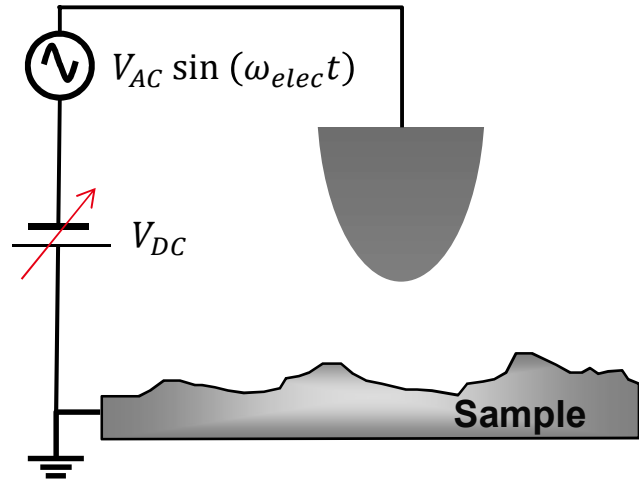
- **Principe**

- Excitation bimodal autour de la fréquence de résonance ($f_0 \pm f_{mod}$)
- Mesure simultanée des amplitudes correspondantes → variation monotone de la différence (ΔA)
- Une boucle de contre-réaction annule ΔA en ajustant la fréquence de résonance f_0

- **Applications**

- Piezo Force Microscopy (PFM)
- Contact resonance (CR-AFM)
- Kelvin force microscopy (KFM)
- EFM ...

KFM en mode DFRT



- Acquisition en mode AM-KFM → suivi de la fréquence de résonance en mode DFRT

$$V = V_{DC} - V_{CPD} + V_{AC} \sin(\omega_{elect} t)$$

Force électrostatique

$$F_{\omega_{elec}} = \frac{\partial C}{\partial z} (V_{DC} - V_{CPD}) V_{AC}$$

- Annulation de la composante à ω_{elec} de la force électrostatique
 - $V_{DC} = V_{CPD}$

Simple passage

Excitation mécanique à la
résonance du levier ($f_{méca} = f_0$) +
Excitation bimodal à $f_{élec} \pm f_{mo} =$
 $f_1 \pm f_m$

Tapping (Air)
ou
nc-AFM (Vide, UHV)



Modulation électrique $f_{élec} = f_1$

Démodulation à $f_{élec} \rightarrow$ amplitude

Double passage

1^{er} passage

Excitation mécanique à la
résonance du levier ($f_{méca} = f_0$) +
Excitation bimodal à $f_{élec} \pm f_{mod} =$
 $f_1 \pm f_m$

Tapping (Air)
ou
nc-AFM (Vide, UHV)

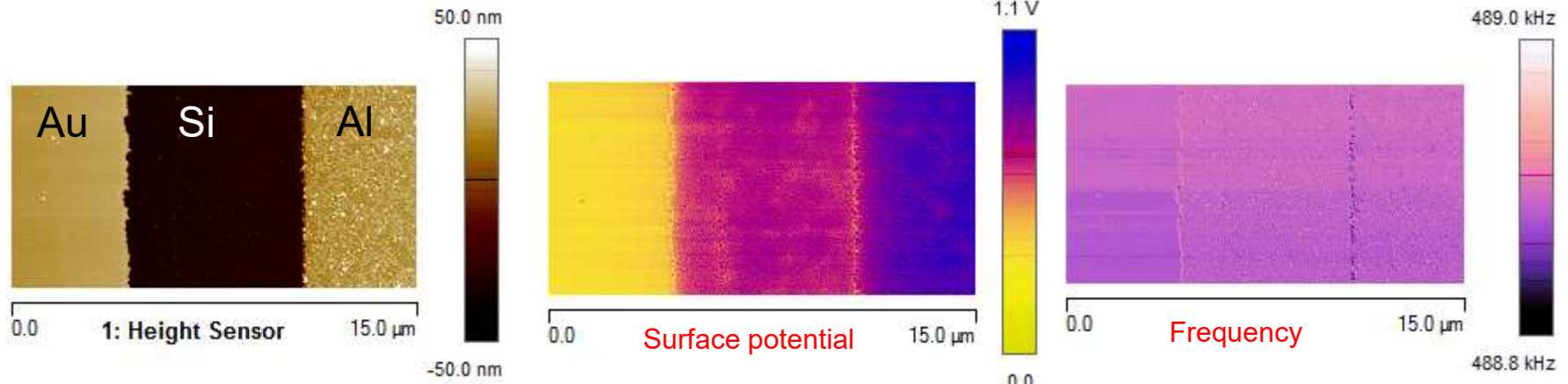
2^{ème} passage : lift

Modulation électrique $f_{élec} = f_1$

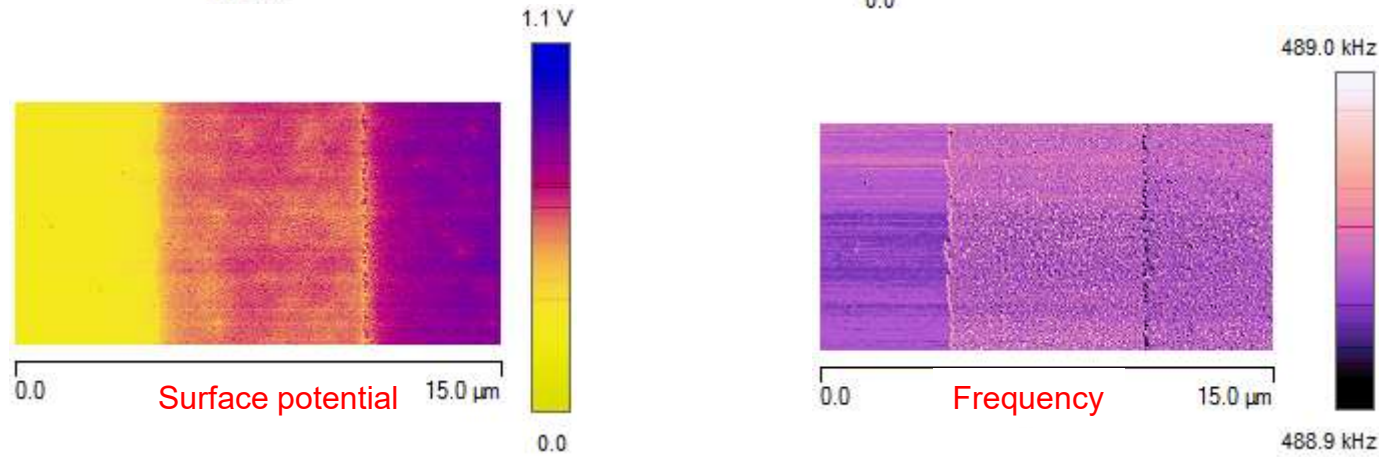
Démodulation à $f_{élec} \rightarrow$ amplitude
Hauteur de lift (20 à 100 nm)

EXEMPLE

DFRT KFM : $V_{ac}=500$ mV, sideband: 9 mV, 1.5 KHz



AM-KFM
 $V_{ac}=500$ mV,
488.6 KHz



« EFM »-DFRT
 $V_{dc}=0V$
sideband: 9 mV, 1.5 KHz



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Modulation d'Amplitude (AM) vs Modulation de Fréquence (FM)

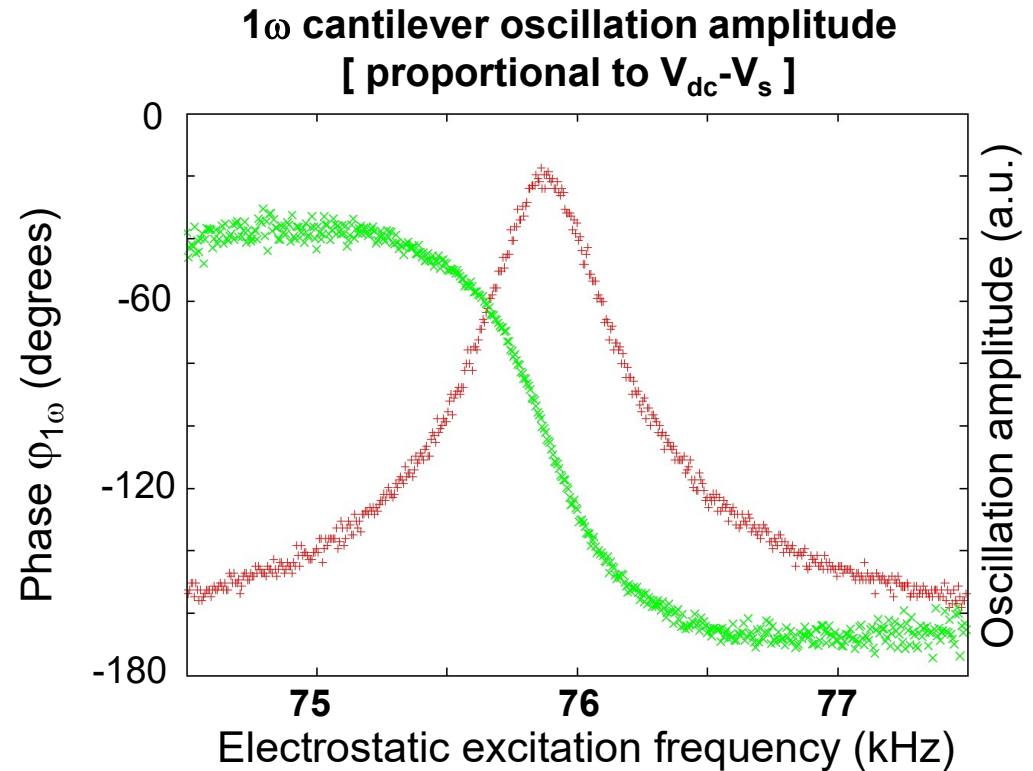
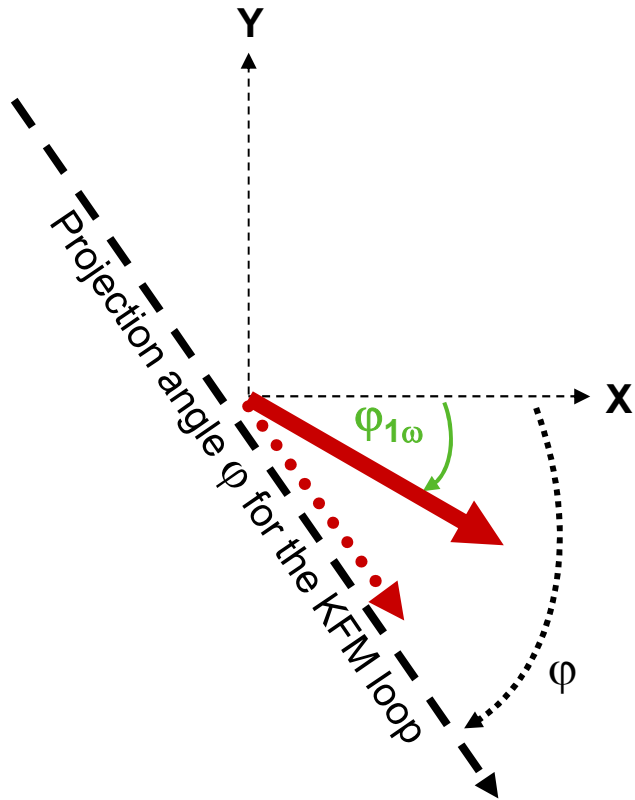
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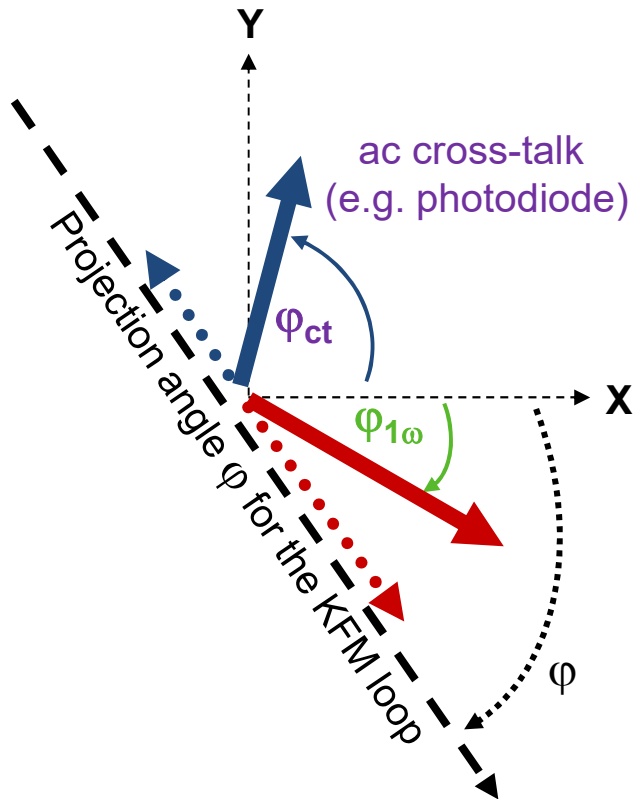
Practical operation principle



projection angle necessary for the KFM feedback loop

$$\text{KFM "equation" : } dC/dz \cdot (V_{dc}-V_s) \cdot V_{ac} \cdot \cos(\phi_{1\omega}-\phi) = 0$$

Practical operation principle ... with ac cross-talks



KFM "equation"

$$\frac{dC}{dz} \cdot (V_{dc} - V_s) \cdot V_{ac} \cdot \cos(\phi_{1\omega} - \phi) + A_{ct} \cdot V_{ac} \cdot \cos(\phi_{ct} - \phi) = 0$$

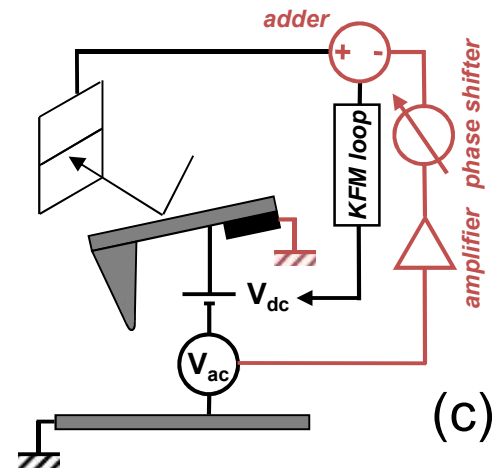
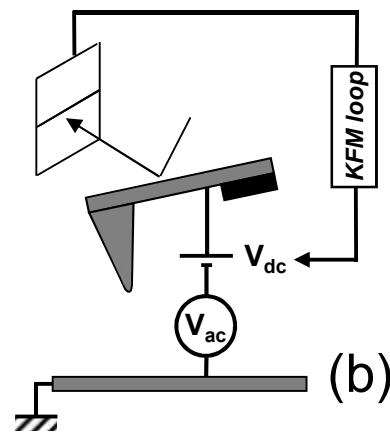
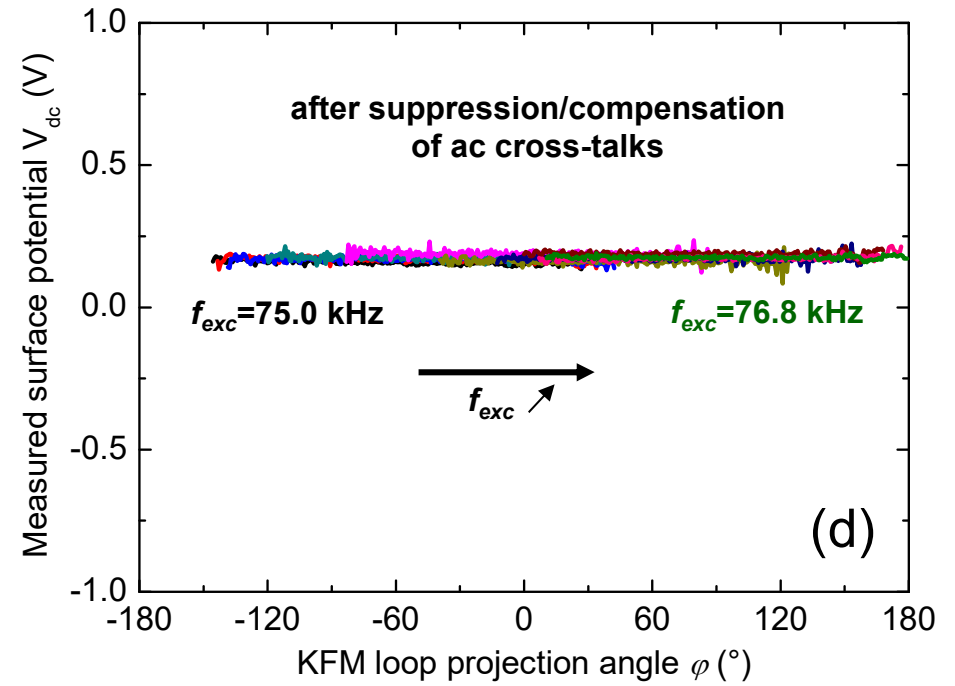
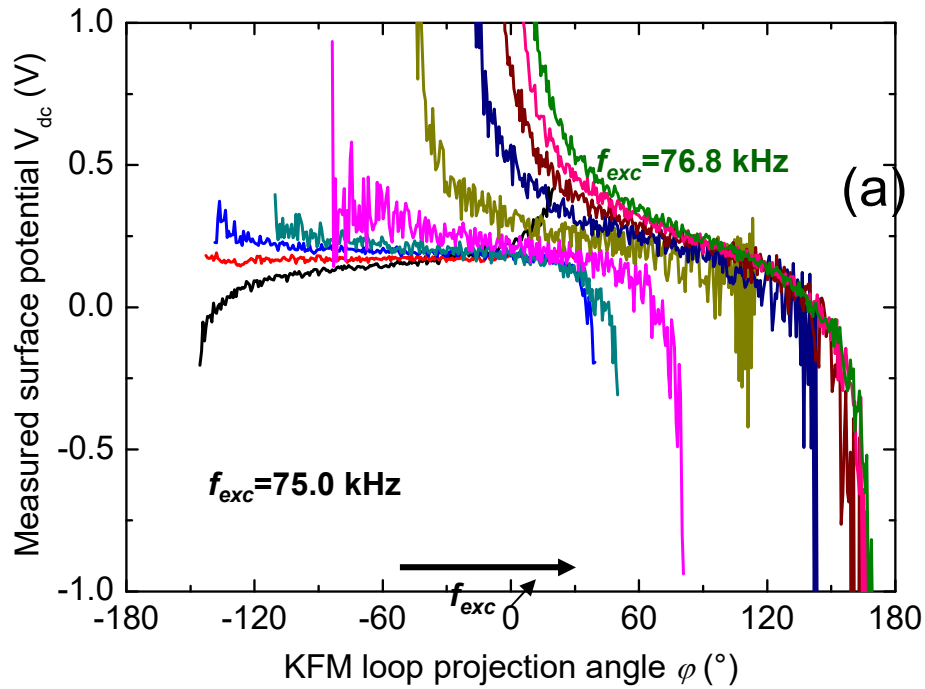
$$V_{dc} = V_s + \underbrace{A_{ct} \cdot \cos(\phi_{ct} - \phi) / \frac{dC}{dz} \cos(\phi_{1\omega} - \phi)}$$

This term depends ☹ ☹ ☹

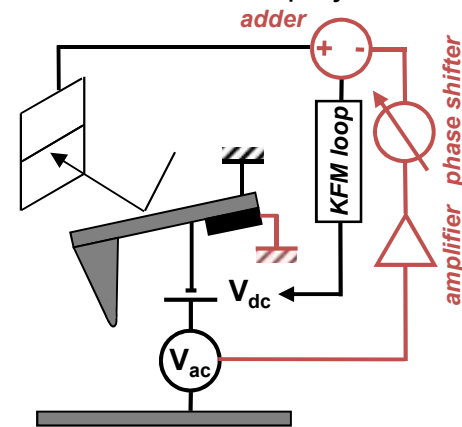
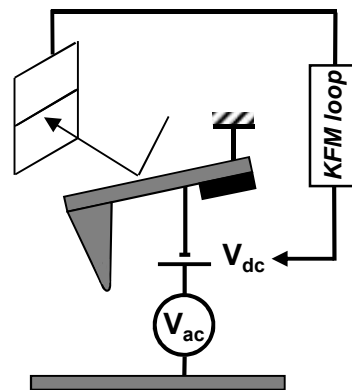
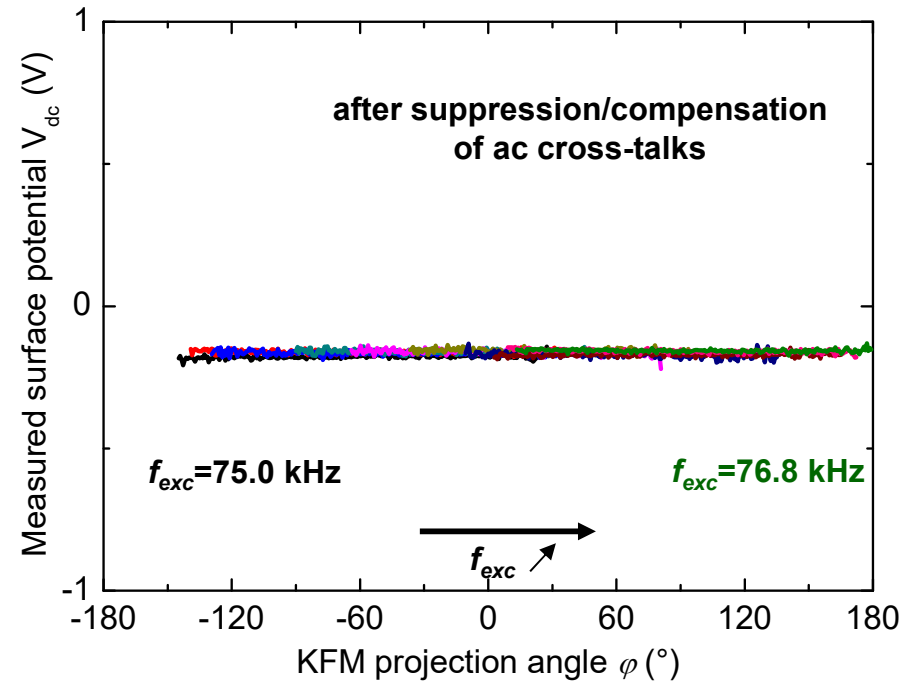
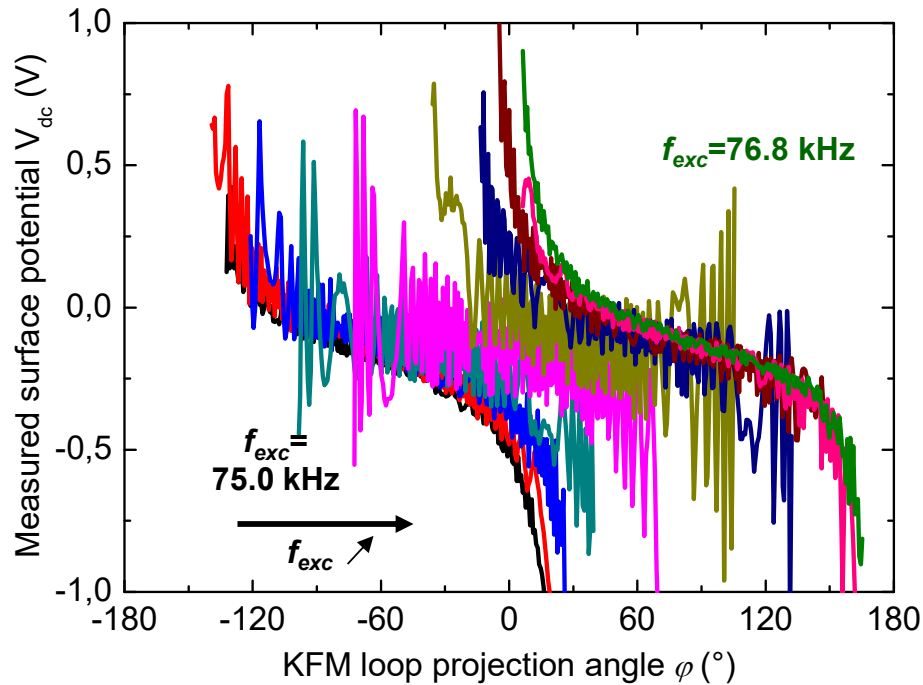
- on ϕ ("drive phase")
- on $\phi_{1\omega}$ (excitation frequency)
- on z (via dC/dz)

In practice (Brüker) : photodiode + mechanical ac-cross-talks

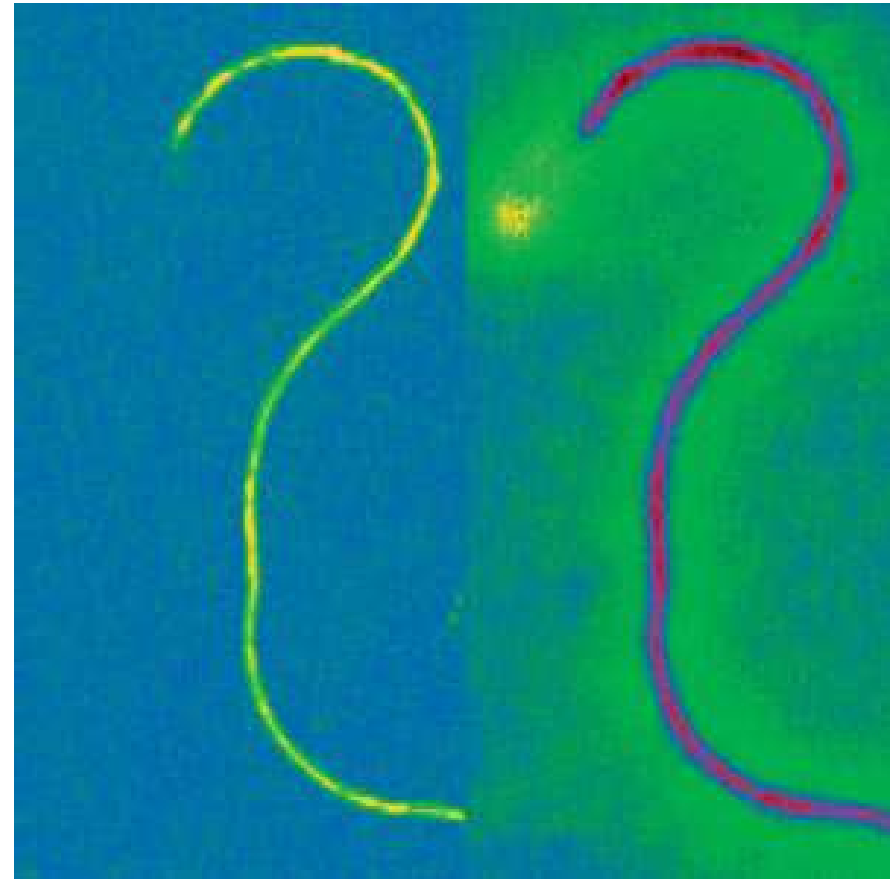
Cross-talk suppression/compensation



Cross-talk suppression/compensation



Questions ?



MICROSCOPIE EFM/KFM : CONFIGURATIONS SIMPLE PASS

	EFM	Modulation d'Amplitude			Modulation de fréquence	
		KFM	DFRT	OL-KFM	KFM	OL-KFM
Topographie	en mode Tapping (air) ou en mode non-contact (ultra-vide)					
Simple Passage	✗	✓	✓	✓	✓	✓
Excitation mécanique $f_{méca}$	✗	f_0	f_0 $f_1 \pm f_{mod}$	f_0	f_0	f_0
Modulation électrique $f_{élect}$	✗	f_1 ou hors résonance	f_1	<i>Basse fréquence</i> $\ll f_0$		
Démodulation	✗	Amplitude @ $f_{élect}$		Amplitudes @ $f_{élect}$ et à $2f_{élect}$	Phase @ f_0 puis Amplitude @ $f_{élect}$	Phase @ f_0 puis Amplitudes @ $f_{élect}$ et à $2f_{élect}$

f_0 fréquence fondamentale du levier / f_1 1^{ère} harmonique du levier / f_{mod} fréquence de modulation < 2 kHz

MICROSCOPIE EFM/KFM : CONFIGURATIONS DOUBLE PASS

	EFM	Modulation d'Amplitude			Modulation de fréquence	
		KFM	DFRT	OL-KFM	KFM	OL-KFM
Topographie	en mode Tapping (air) ou en mode non-contact (ultra-vide)					
Double Passage	✓	✓	✓	✓	✓	✓
Excitation mécanique $f_{méca}$ (1 ^{er} passage)	f_0	f_0	f_0	f_0	f_0	f_0
Excitation mécanique $f_{méca}$ (2 ^{ème} passage)	f_0	-	$f_0 \pm f_{mod}$ ou $f_1 \pm f_{mod}$	-	f_0	f_0
Modulation électrique $f_{élect}$ (2 ^{ème} passage)	-	f_0 ou f_1 ou hors résonance	f_0 ou f_1	<i>Basse fréquence</i> $\ll f_0$		
Démodulation	Phase @ f_0	Amplitude @ $f_{élect}$		Amplitudes @ $f_{élect}$ et à $2f_{élect}$	Phase @ f_0 puis Amplitude @ $f_{élect}$	Phase @ f_0 puis Amplitudes @ $f_{élect}$ et à $2f_{élect}$

f_0 fréquence fondamentale du levier / f_1 1^{ère} harmonique du levier / f_{mod} fréquence de modulation < 2 kHz

RÉFÉRENCES

- **S. Sadewasser and Thilo Glatzel « Kelvin probe force microscopy » Springer 2012**
- **B. Bushan « Scanning probe microscopy in nanoscience and nanotechnology » Springer 2009**
 - Chapter 4 Electrostatic Force Microscopy and Kelvin Force Microscopy as a Probe of the Electrostatic and Electronic Properties of Carbon Nanotubes